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Aberdeen SMER SC006

20th August 2013



Overview

- Background
- Error Description
 - Analysis of flow data
- Initial Tests
- Carrier Checks
- Carrier Data Plates
- Orifice Plate Photographs
- On-site Testing
- CFD Analysis
- Results
- Summary of Error Periods

Background

- Orifice plate meters are used to accurately measure mass flow rate
 - The orifice plate creates a pressure drop (Δp) related to flow rate (q_m)

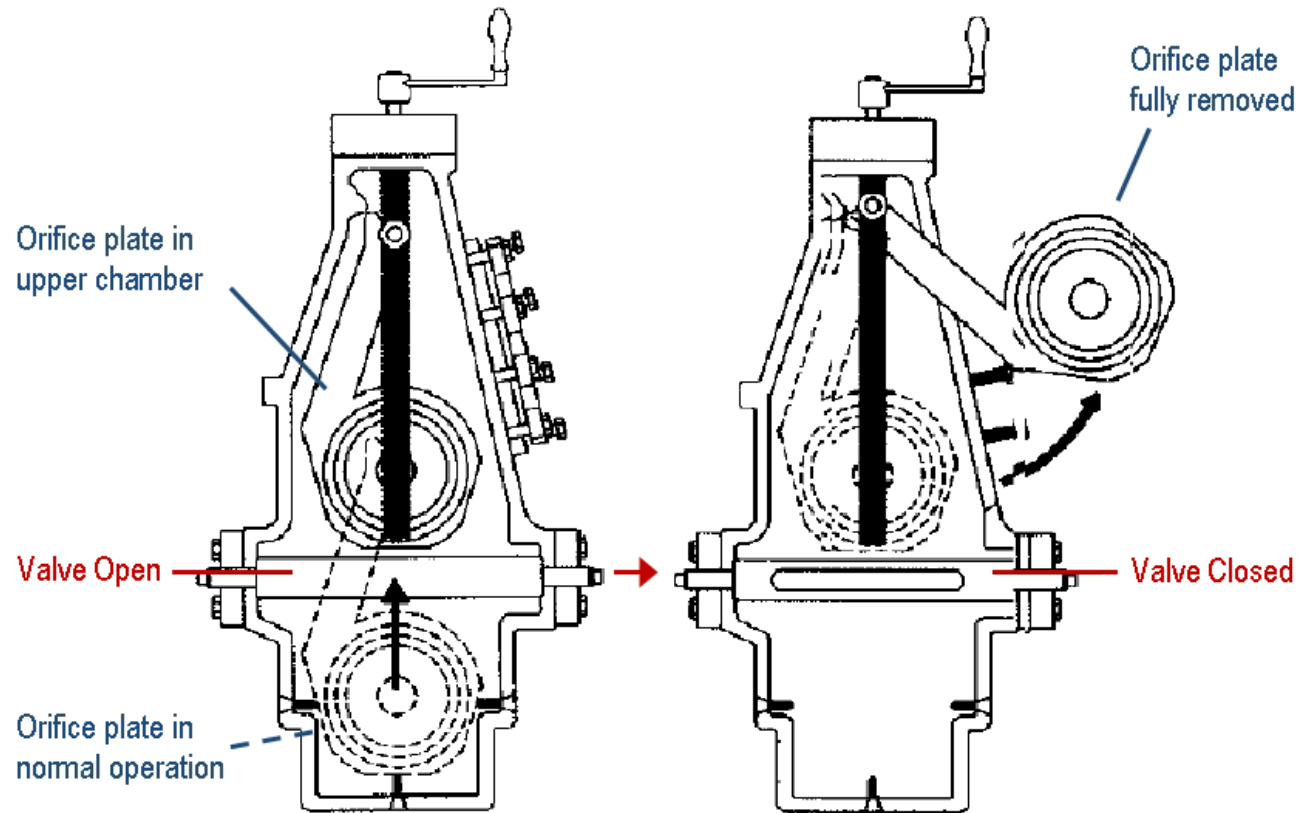
$$q_m = \frac{C}{\sqrt{1-\beta^4}} \varepsilon \frac{\pi}{4} d^2 \sqrt{2\Delta p \rho_1}$$

- This calculation is carried out within a dedicated flow computer algorithm
 - In accordance with ISO 5167-1:1991
- It assumes that the plate is located concentrically within the pipe
- If the plate is located eccentrically then the equation is not valid
 - Tolerance in this case is 0.5 mm
 - (or up to 1.0 mm with 0.3% additional uncertainty)
 - Some further guidance exists up to 12.8 mm eccentricity

Background

- The orifice plate is typically placed inside a carrier mechanism
 - To enable accurate location of the orifice plate within the pipe
- This carrier is designed to allow maintenance on the orifice plate without venting the metering pipe work
 - Two chambers separated by a valve
- This carrier is unusual in design because the valve is open during service

Background



Error Description

- 7th August 2010 - Fault logged
 - 'Possible metering issues' following line pack calculations
- 10th August 2010 - Advised that the orifice plate was not set correctly
 - DP of 54 mbar was showing as 6 mbar
 - Flow of 1.42 Mscm/d was shown as 0.5 Mscm/d
- Subsequent interviews with mechanical operatives provided some confidence that the counter was set at 99950 following the orifice plate change on 27th July 2010
- Unable to confirm counter reading at start of orifice plate change on 27th July 2010
- Unable to confirm counter reading at orifice plate change on 21st July 2009

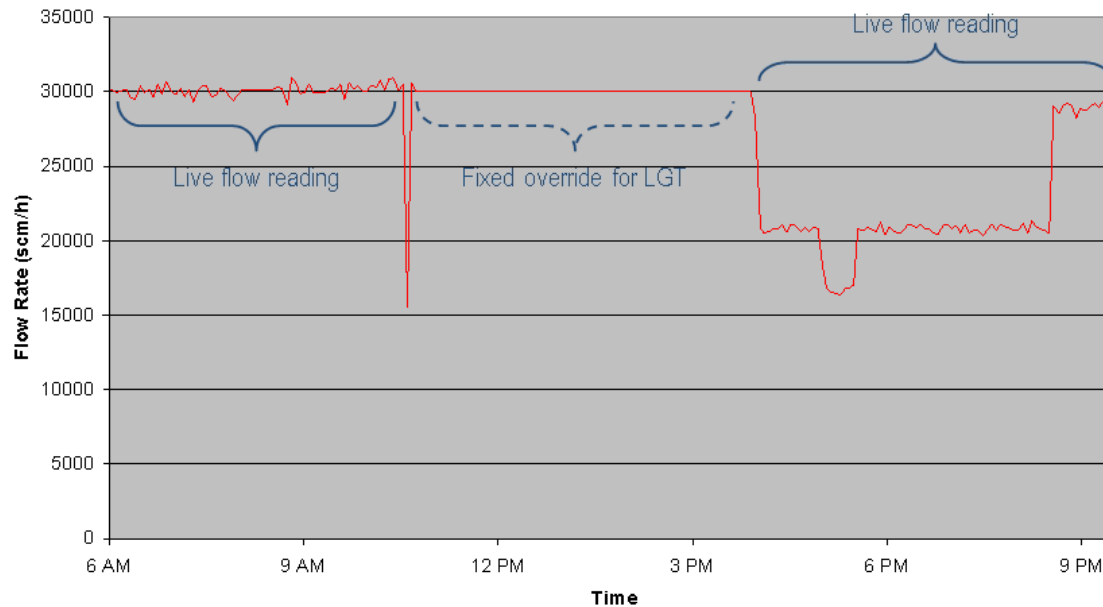
Error Description

- Site controlled to flow rate set point and pressure overrides
- During normal orifice plate changes the flow control valve is set to direct valve control to prevent movement of the valve due to spurious signals
- On 21st July 2009 and 10th August 2010 a step change in flow rate can be seen
- On 27th July 2010 the flow rate was transient
 - Flow rate was not maintained because of minimal pressure differential across the site
- On 5th August 2008 there was no change in flow rate

Error Description

- 21st July 2009 – Problem was introduced at orifice plate change
 - ~30 kscm/h site flow prior to plate change
 - ~21 kscm/h site flow following plate change
 - Indicates an under-registration of 31 % following change

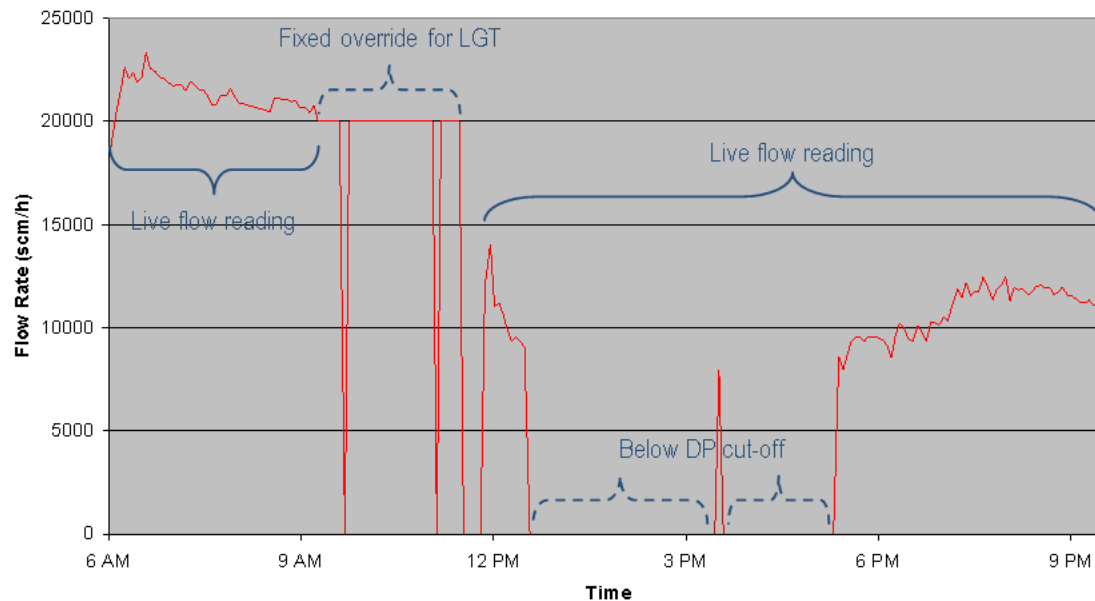
Flow Profile 21st July 2009



Error Description

- 27th July 2010 – Orifice plate was changed
 - Transient flow rate before and after plate change
 - No direct comparison available
 - DP was close to the low cut-off and some zero flow rates were recorded

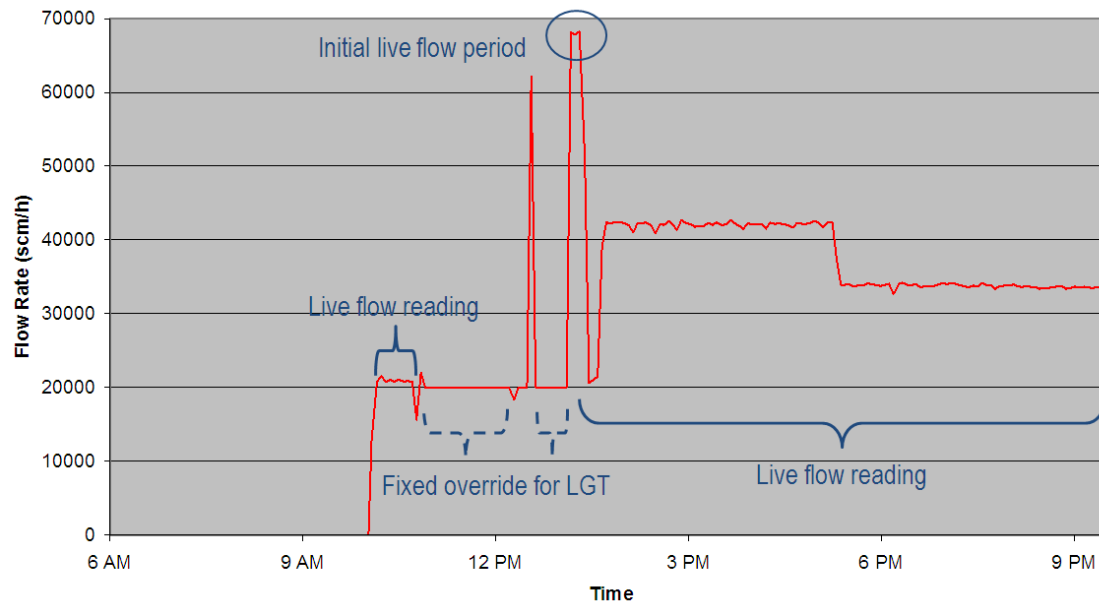
Flow Profile 27th July 2010



Error Description

- 10th August 2010 – Fault corrected
 - ~21 kscm/h site flow prior to correction
 - ~68 kscm/h site flow following correction
 - Indicates an under-registration of 69 % before correction

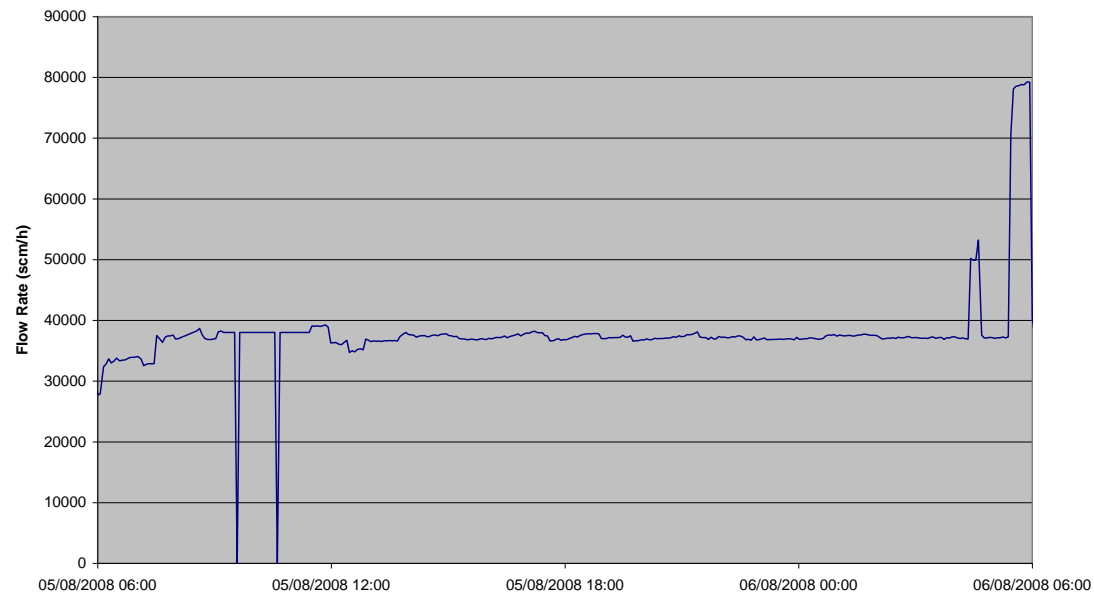
Flow Profile 10th August 2010



Error Description

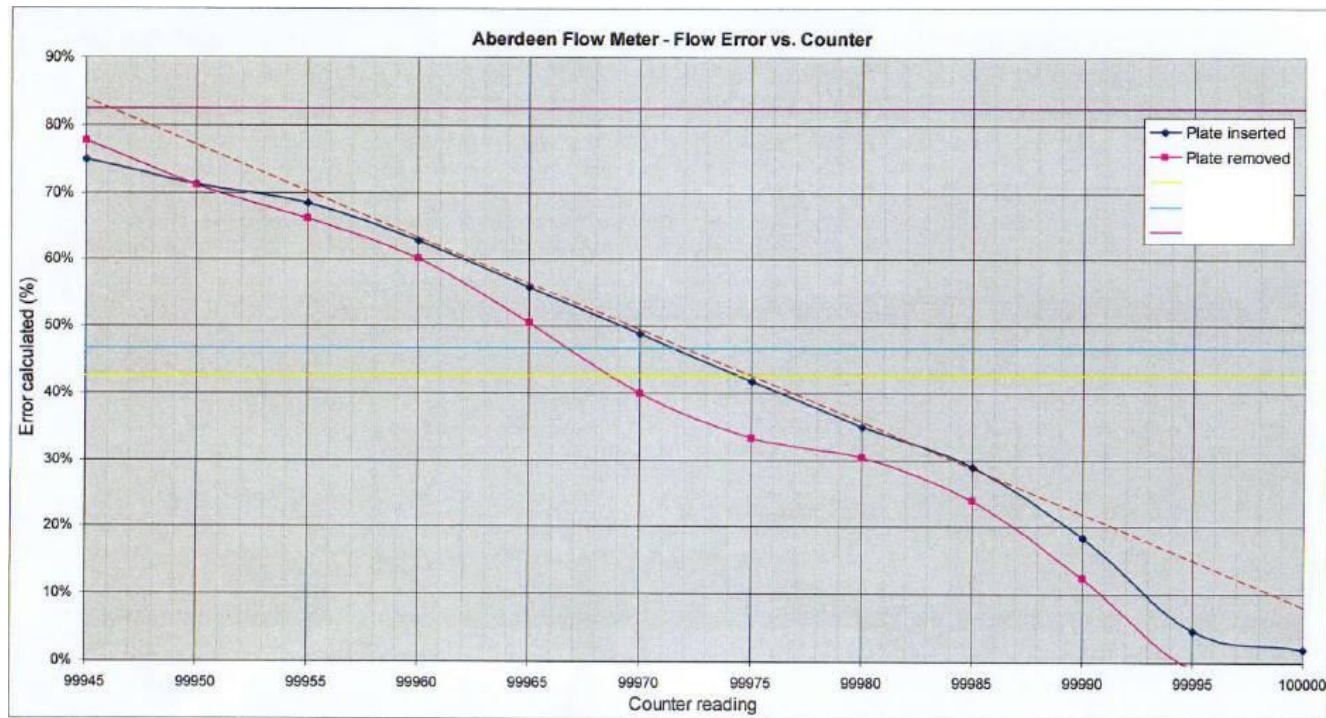
- 5th August 2008 – Correct orifice plate change
 - ~38 kscm/h site flow prior to plate change
 - Fixed flow (38 kscm/h) recorded for duration of plate change
 - ~38 kscm/h site flow following plate change

Flow Profile 5th August 2008



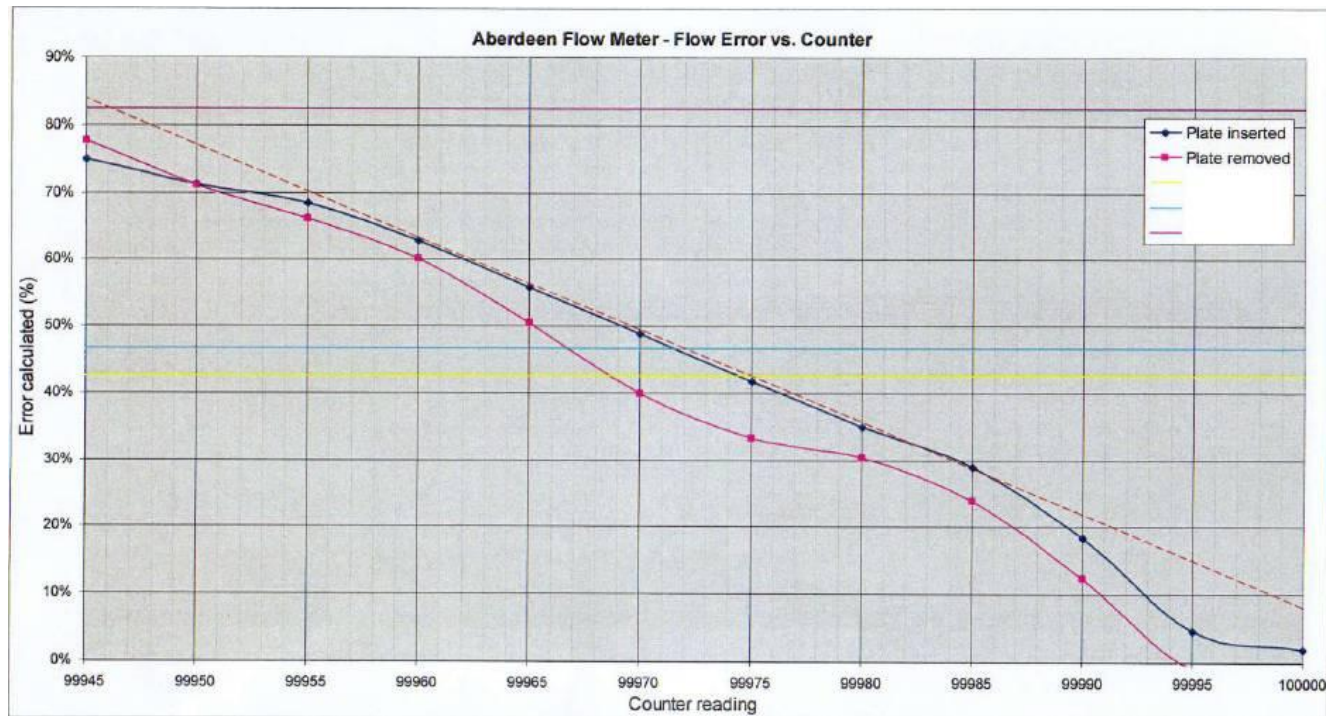
Initial Tests

- Initial tests were carried out by downstream party to estimate error magnitude
 - Prior to appointment of ITE
 - Not suitable as quantification of error



Initial Tests

- Error at 99950 counter reading shown as 71%
 - Compares well with 69% estimated from step change
- Step change of 31% suggests that the unknown counter reading is ~99984



Carrier Checks

- Aimed to determine the relationship between the counter reading and the physical location of the plate within the pipe
- Downstream spool removed
- Vertical and horizontal offsets measured
 - Using slip gauges
 - At various counter readings on removal and insertion

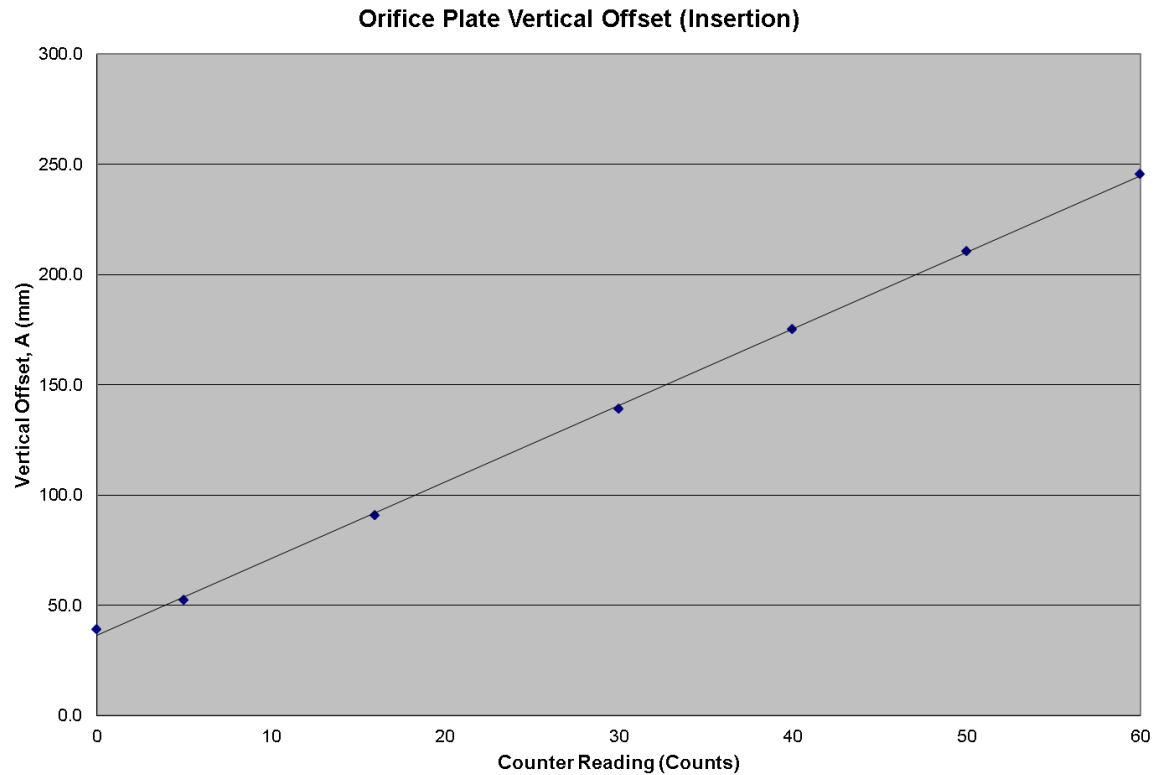
Carrier Checks

- 00000 Correct location (top right)
- 99950 Correct location (bottom right)
 - Offset of 173.0 mm
- 99984 Correct location (bottom left)
 - Offset of 51.3 mm



Carrier Checks

- Linear profile



Carrier Checks

- Average of three readings
- 99950 - No difference in readings
- 99984 - Standard deviation less than half of the measurement uncertainty
- Good repeatability

Carrier Data Plates

- Identification plate
 - Serial number and carrier specification
- Information plate
 - Step by step Instructions on removal and insertion of orifice plate
 - Not easily readable



Carrier Data Plates

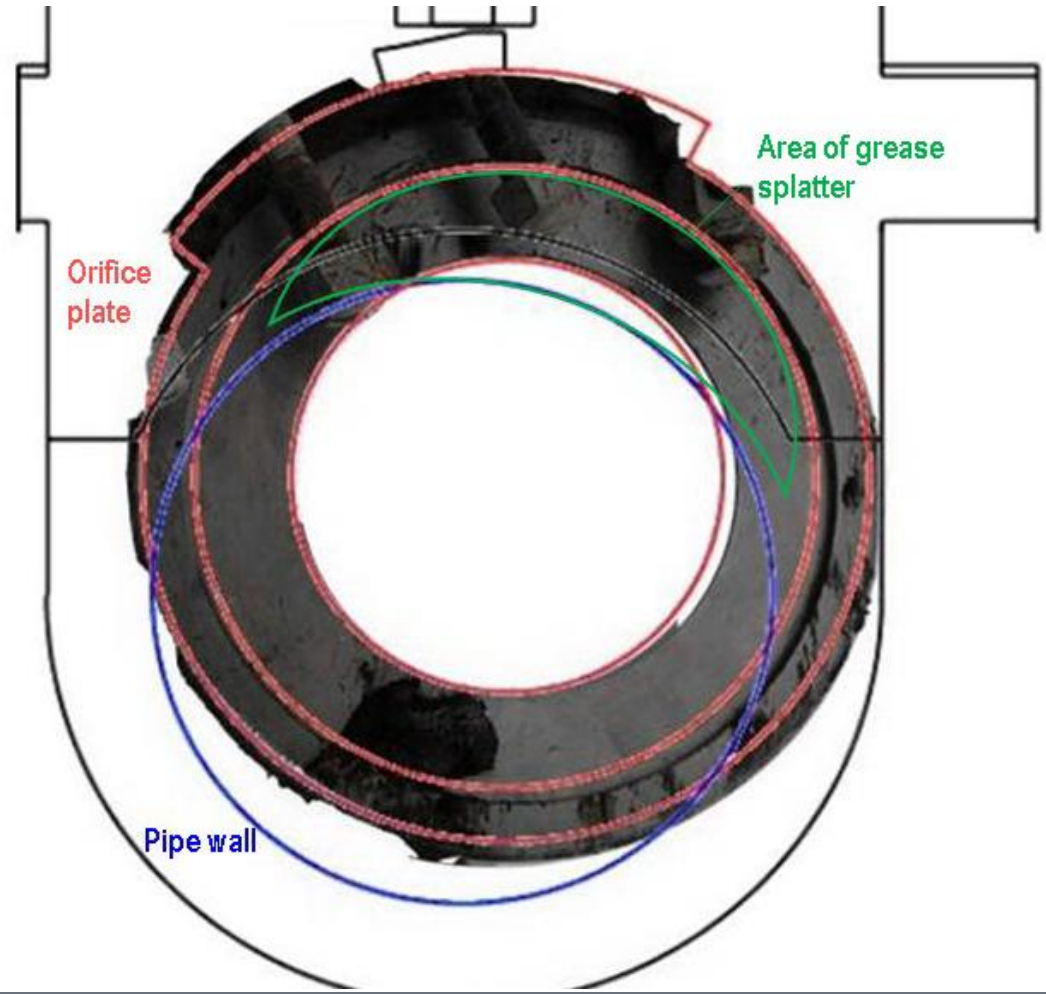
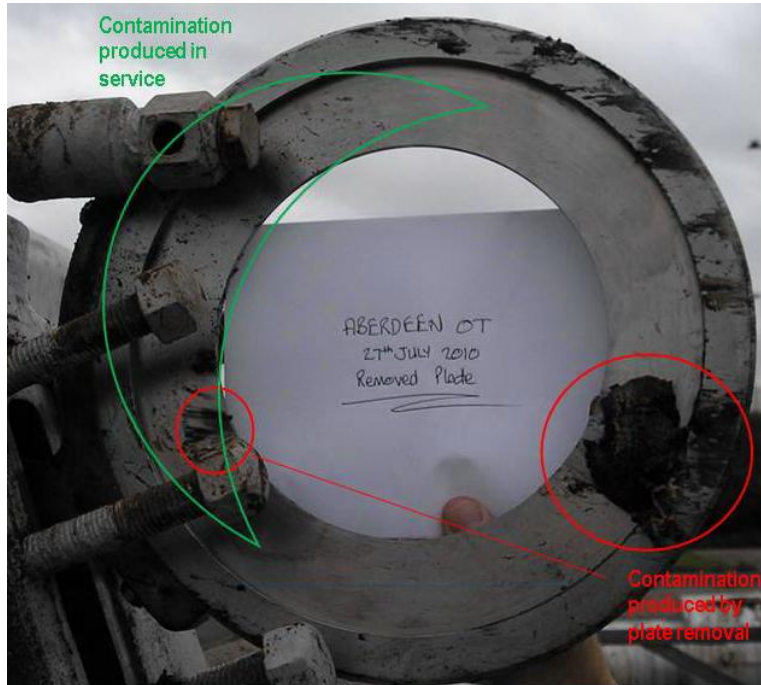
- The information plate states that the fully inserted position should be at a counter reading of between 9995 and 0005
 - Five digit counter
 - Fully inserted position is exactly 00000
- From this it can be seen that the four digit 9995 counter reading was likely to have been misinterpreted as a five digit reading of 99950
- No evidence to support a counter reading of 99984 (estimated from initial analysis)
- However it was thought that the 99885 which is stamped in two locations on the carrier information plate could have been misread as 99985

Orifice Plate Photographs

- Photographic records are kept of each plate (both faces) on insertion and removal
- Plate removed on 21st July 2009 was clean
- Plate removed on 27th July 2010 showed some contamination
 - Location supports 99985 counter reading
- Plate removed on 29th July 2011 showed some contamination
 - Pattern consistent with normal flow conditions
 - No significant effect based on quantity and location

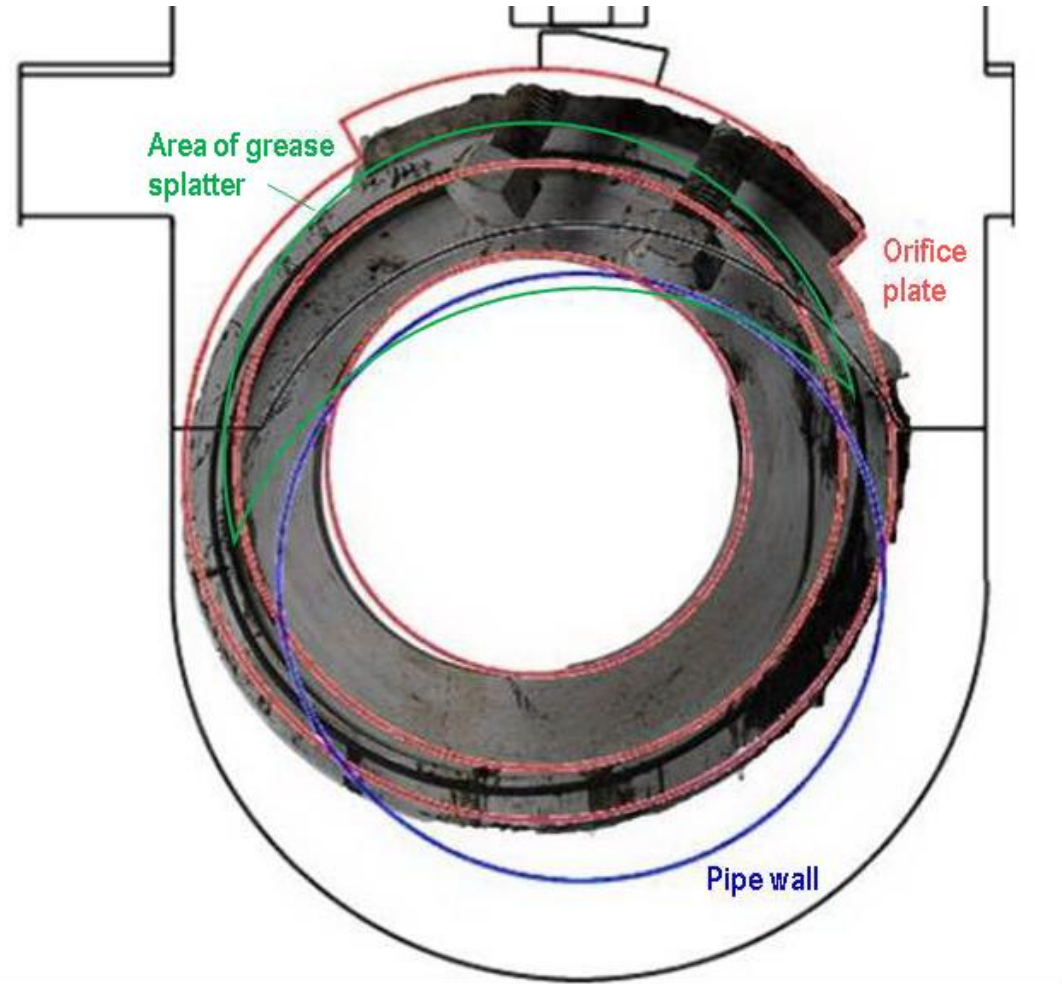
Orifice Plate Photographs

- July 2010, Upstream



Orifice Plate Photographs

- July 2010, Downstream

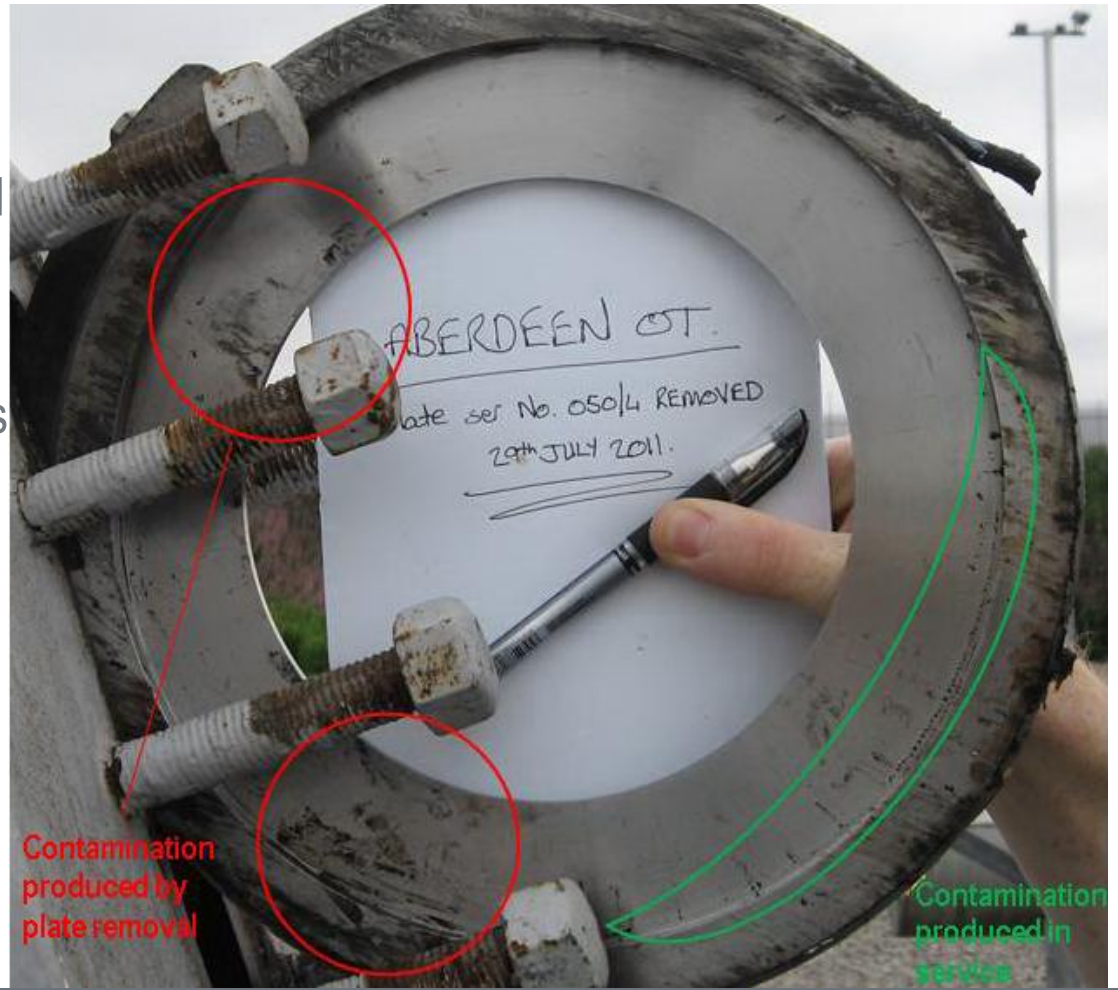


Orifice Plate Photographs

- The splatter pattern suggests small amounts of grease being picked up and deposited by a flow of gas
- Contamination of this kind would be removed by the flow of gas under normal operating conditions (higher flow rates), particularly around the bore edge
- This is an indication that normal gas flows were not experienced by this part of the orifice plate

Orifice Plate Photographs

- July 2011, Upstream
- Typical of minor contamination experienced in service
- Confined to outer annulus
- Streaking radially outwards



On-site Testing

- Aim to establish the relationship between DP and the counter reading at various flow rates and pressures
- Designed to cover the true range experienced during the error period
- Pressure - 54.8 barg to 66.5 barg
- Site maximum flow - 4.5 Mscm/d
- Minimum flow rate - 1.0 Mscm/d
 - Selected because of high uncertainties at lower flow rates

On-site Testing

- Problems achieving desired pressures in upstream National Transmission System
- 15th February 2012 the pressure was between 61.4 barg and 62.1 barg
 - Selected as intermediate pressure point
- Aimed to test at 66 barg and 55 barg
 - It was suggested that 57 barg was a more achievable target
- 18th April 2012 the pressure was between 63.6 barg and 64.0 barg
 - Selected as high pressure point
- 19th April 2012 the pressure was between 58.1 barg and 58.7 barg
 - Selected as low pressure point
- Pressure range was deemed to be acceptable as it covered >85% of the data
 - Later shown to be insensitive to pressure

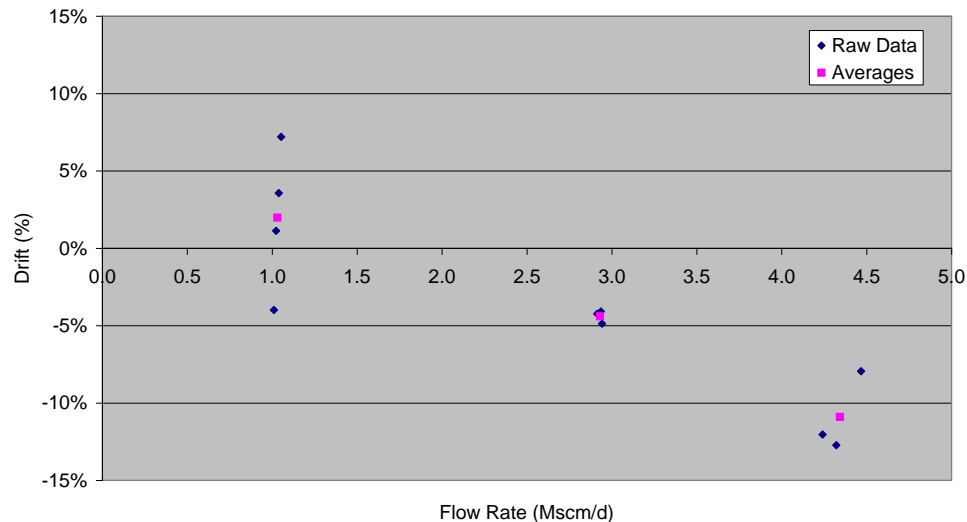
On-site Testing

- Pressure maintained by upstream party
- Set flow control valve in direct valve control to fix flow rate
- Positioned plate at various counter readings (removal and insertion)
- Logged process data (DP, erroneous flow rate, etc)
- Repeated for 3 different flow rates at 3 different pressures
- Some instability in flow rate and pressure (pre- and post-check)

On-site Testing

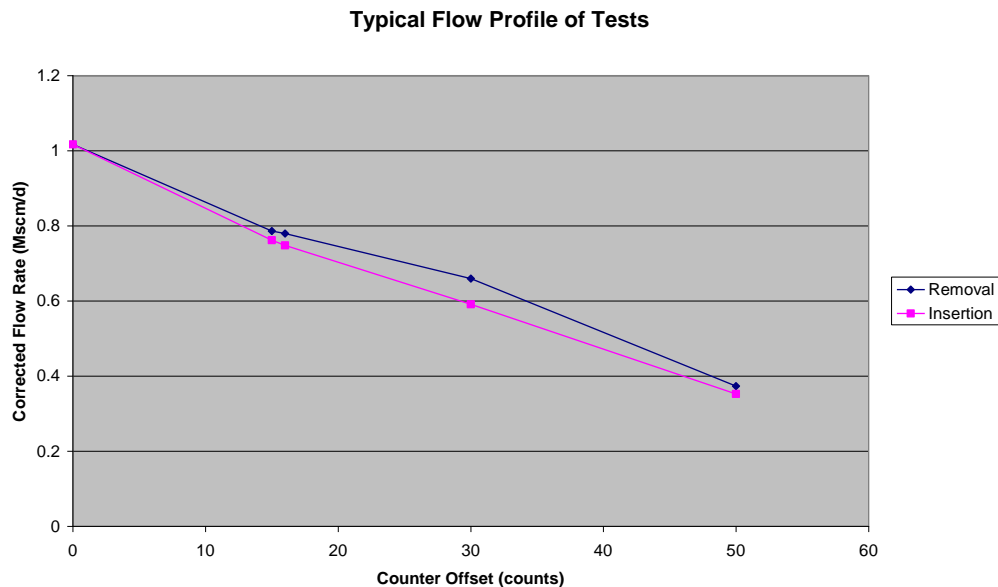
- Flow rate drift was caused by mis-match between the supplied flow rate and the downstream demand (~2 Mscm/d)
- This was most prevalent at the highest flow rates (i.e. where the difference between supply and demand was at it's the greatest)
- Assumed to be linear over the duration of each test

Graph of Drift against Flow Rate



On-site Testing

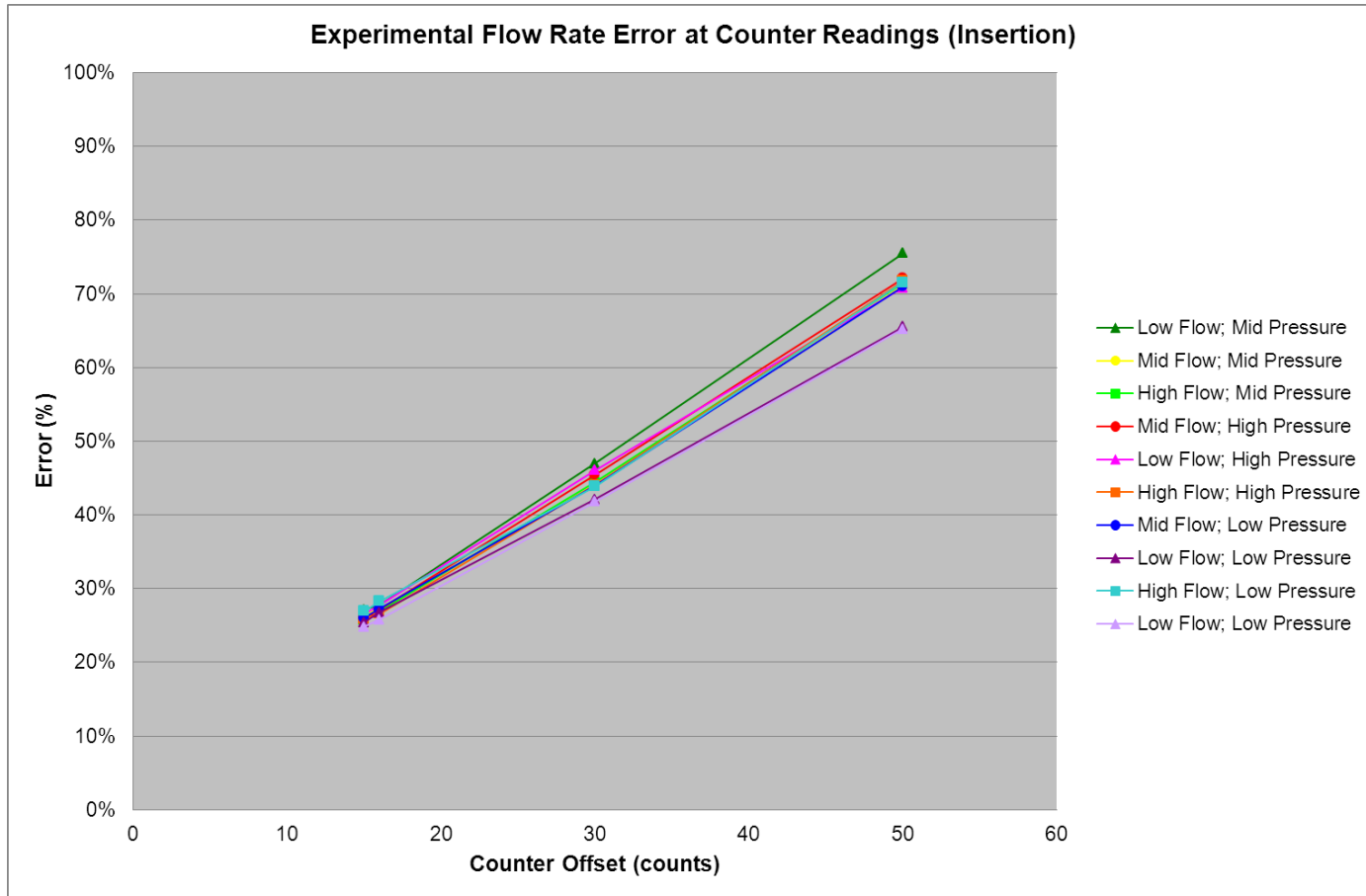
- At each point there was a slight difference in results between removal and insertion due to the difference in direction of the horizontal offset
 - Plate moves towards the differential pressure tapping points on removal and away from them on insertion
- Results in slightly higher flow rates on removal



On-site Testing

- Assumed that orifice plate was inserted to the counter reading, rather than inserted fully and then removed back out to the counter reading.
- It cannot be known for sure, but is more plausible and much more likely

Results - Experimental



CFD Analysis

- No guidance or research for such severe misalignment
- Validation of model
 - Validated against correctly located operating and experimental data
 - Validated against 99970 incorrectly located data
- Results produced for 99985 and 99950 counter readings
 - Experimental DP results not supplied until CFD results were completed
- Recommendations of peer review of analysis report
 - Shorter model (shown to be less accurate)
 - Grid independence checks (completed)
 - 0.1 mm resolution around orifice edge (resolution increased but recommendation not met)
 - Additional reporting requirements (completed)

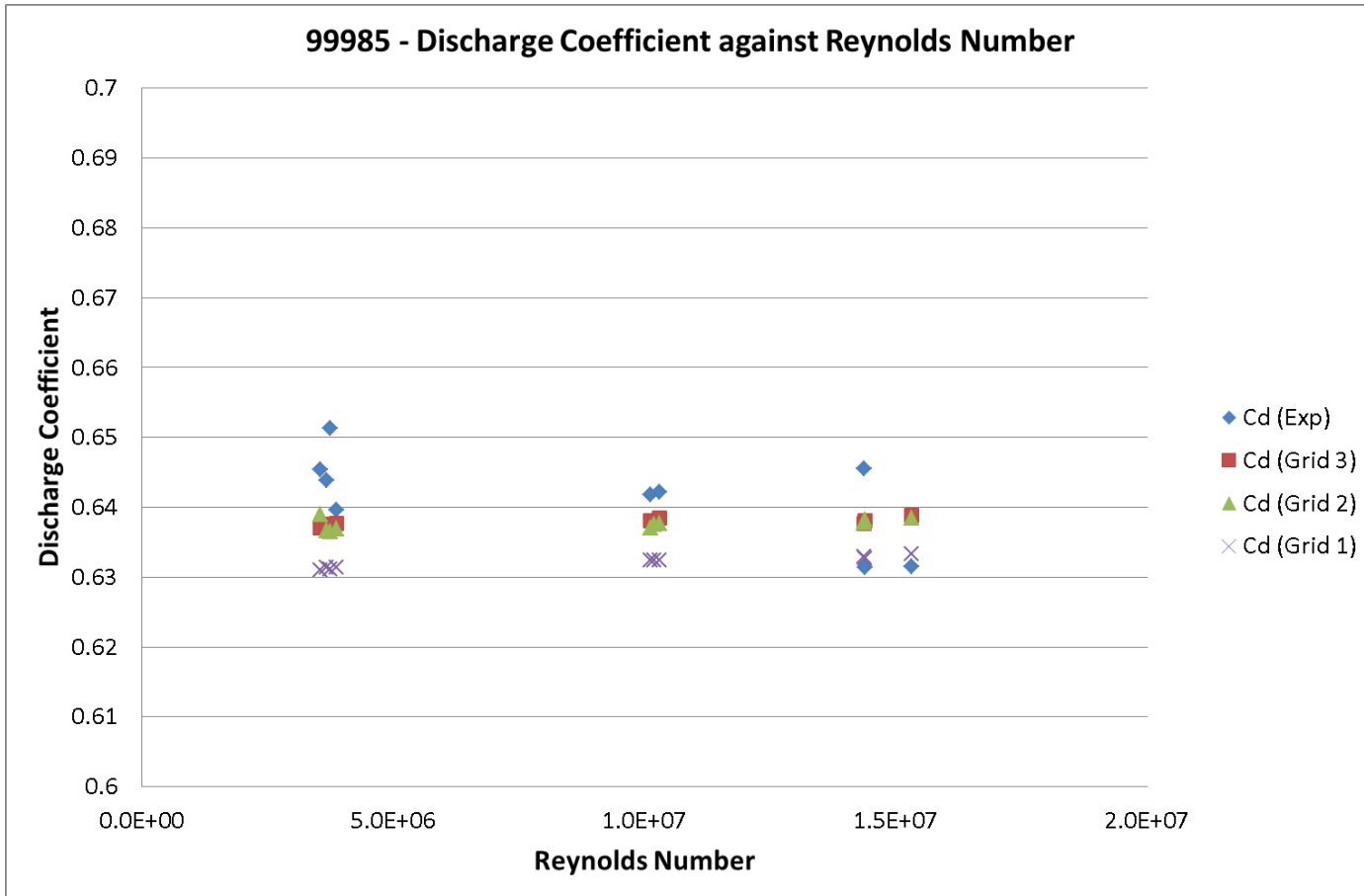
CFD Analysis

- Comparison of CFD and experimental results
 - DP measurement uncertainty used as acceptable tolerance
 - Grid independence considered acceptable under 1%
- 99985 counter reading
 - 7/10 within DP measurement uncertainty
 - Other three were up to 2.5% (vs. 1%)
 - All grid independent (< 0.5%)
- 99950 counter reading
 - 6/10 within DP measurement uncertainty
 - Two others on limit of tolerance (42% vs. 40% and 2.6% vs. 2.5%)
 - Other two were 10% and 4.2% (vs. 6% and 2.5%)
 - All grid independent (< 0.7%)
- All results show error to be independent of process conditions

Results - CFD - 99985

Test	Actual Flow Rate (m ³ /h)	Experimental DP (mbar)	CFD DP (mbar)	Error (%)	DP Measurement Uncertainty (%)
1	594.4561	13.78	14.40	-4.5 %	5.0 %
2	1598.6628	103.14	104.36	-1.2 %	2.0 %
3	2396.1463	242.94	237.43	2.3 %	1.0 %
4	1540.5865	102.49	102.43	0.1 %	2.0 %
6	534.9225	12.06	12.38	-2.7 %	6.0 %
7	2174.3146	208.33	203.99	2.1 %	1.0 %
8	1729.112	112.57	113.87	-1.2 %	1.5%
9	609.996	14.07	14.35	-2.0 %	5.0 %
10	2415.2228	217.58	223.02	-2.5 %	1.0 %
11	648.0378	15.98	16.08	-0.6 %	4.5 %

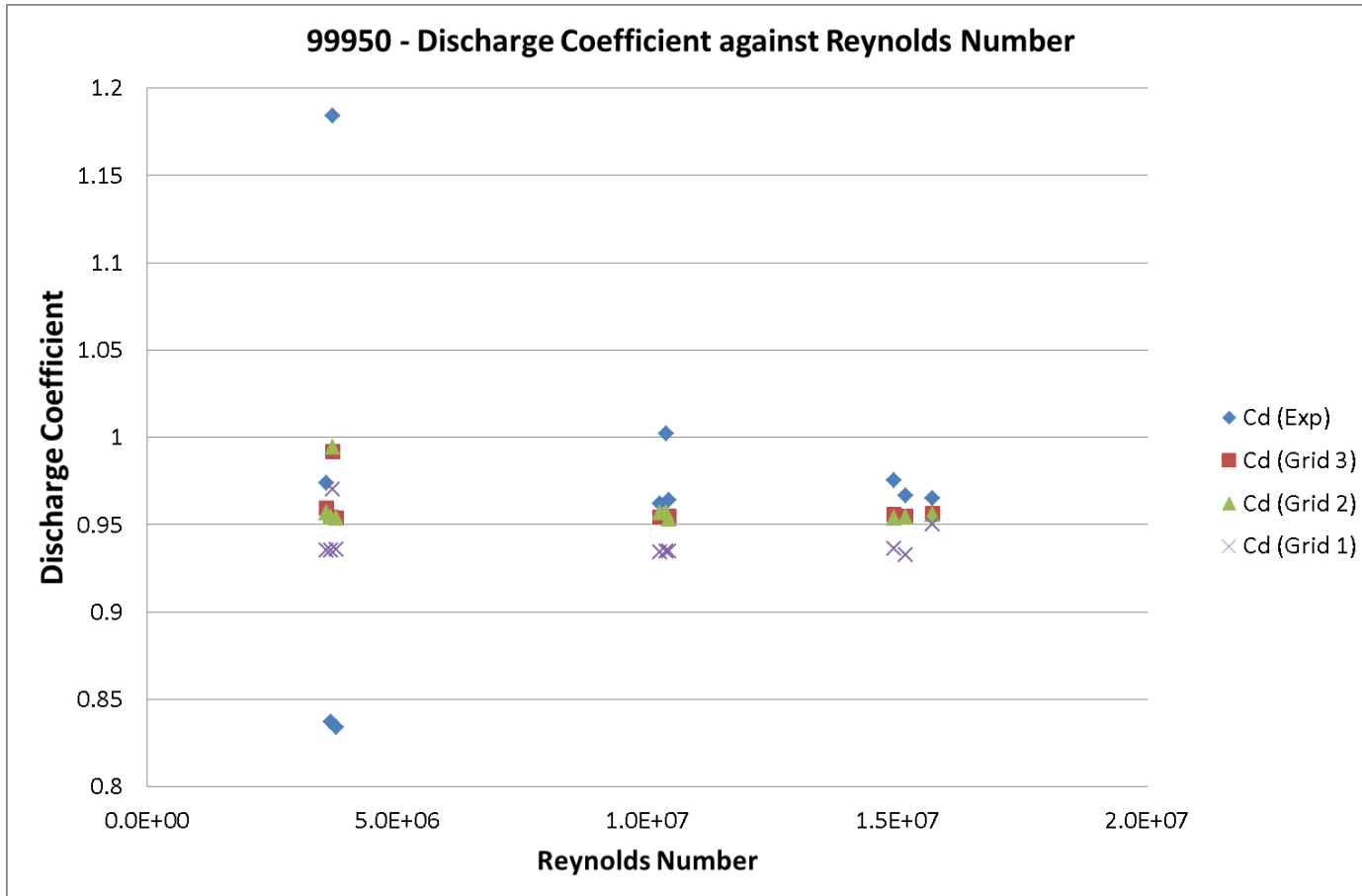
Results - CFD - 99985



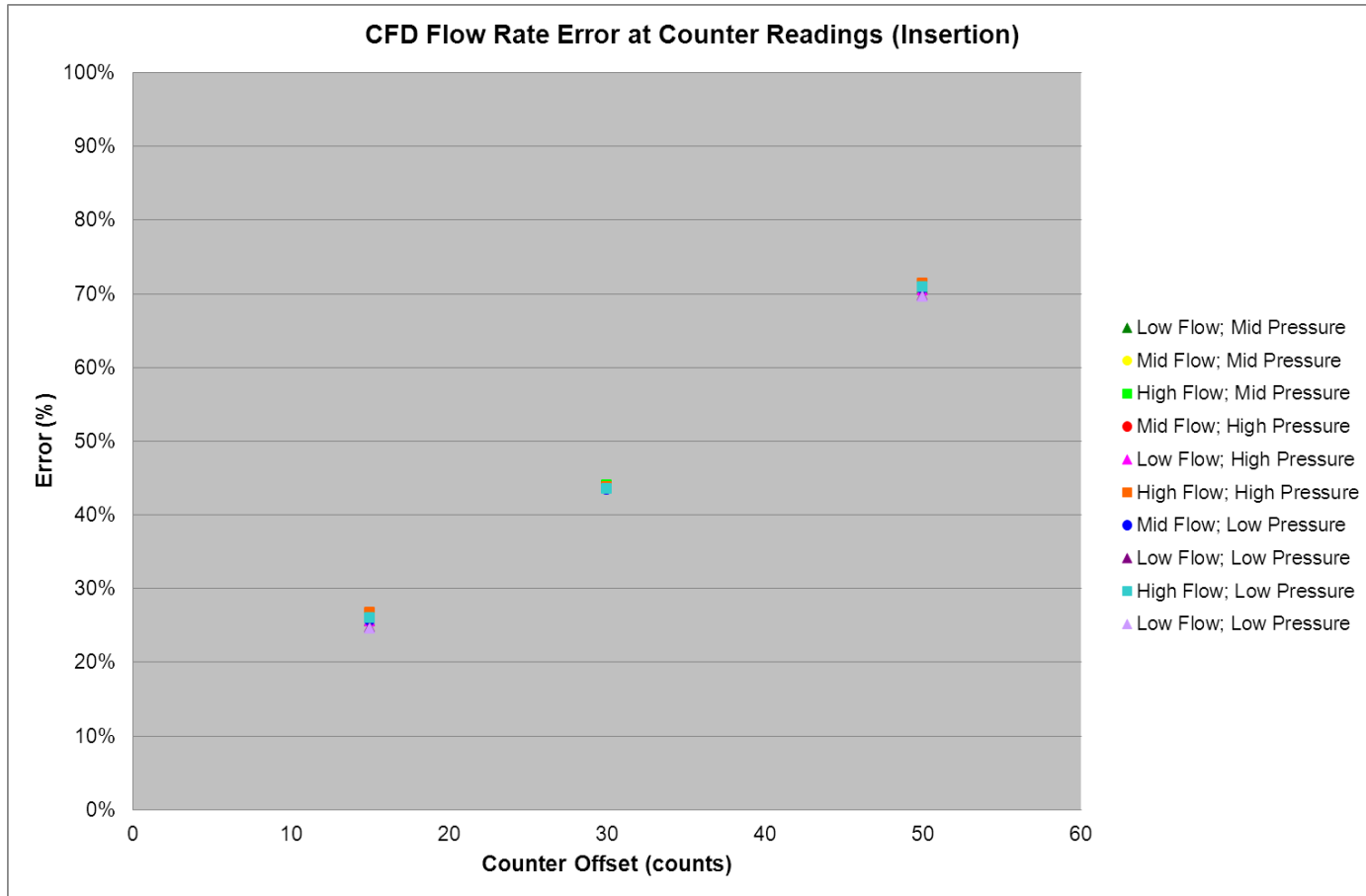
Results - CFD - 99950

Test	Actual Flow Rate (m ³ /h)	Experimental DP (mbar)	CFD DP (mbar)	Error (%)	DP Measurement Uncertainty (%)
1	588.60	1.40	1.99	-42 %	±40 %
2	1619.6945	16.07	16.32	-1.6 %	±5 %
3	2459.8613	37.29	37.98	-1.9 %	±2.5 %
4	1564.3494	14.61	16.09	-10 %	±6 %
6	541.2844	1.85	1.91	-3.2 %	±40 %
7	2284.8572	33.42	34.28	-2.6 %	±2.5 %
8	1748.498	17.43	17.77	-2.0 %	±4 %
9	608.80	2.83	2.18	23 %	±30 %
10	2506.863	34.96	36.43	-4.2 %	±2.5 %
11	633.819	3.07	2.35	23 %	±30 %

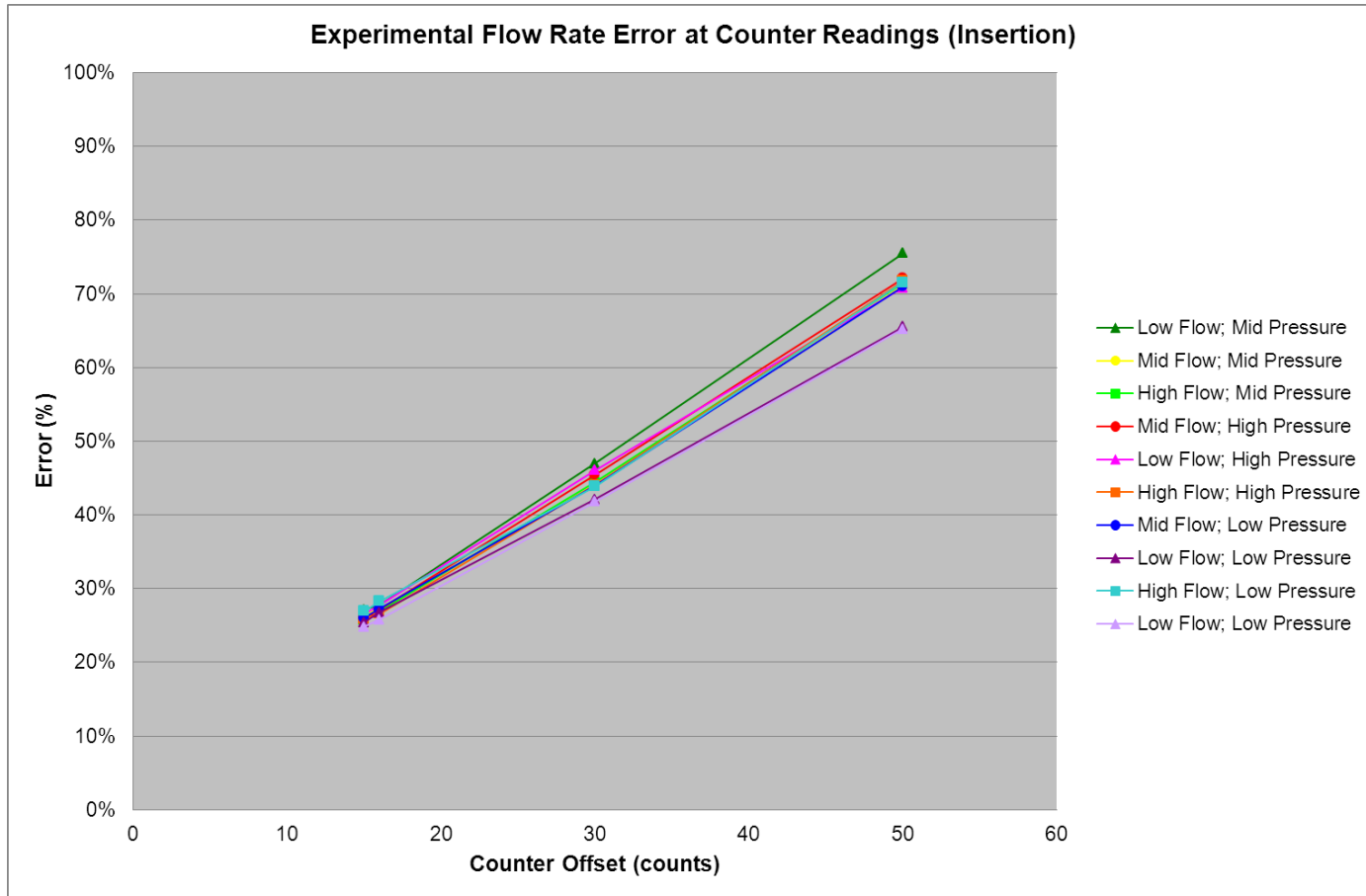
Results - CFD - 99950



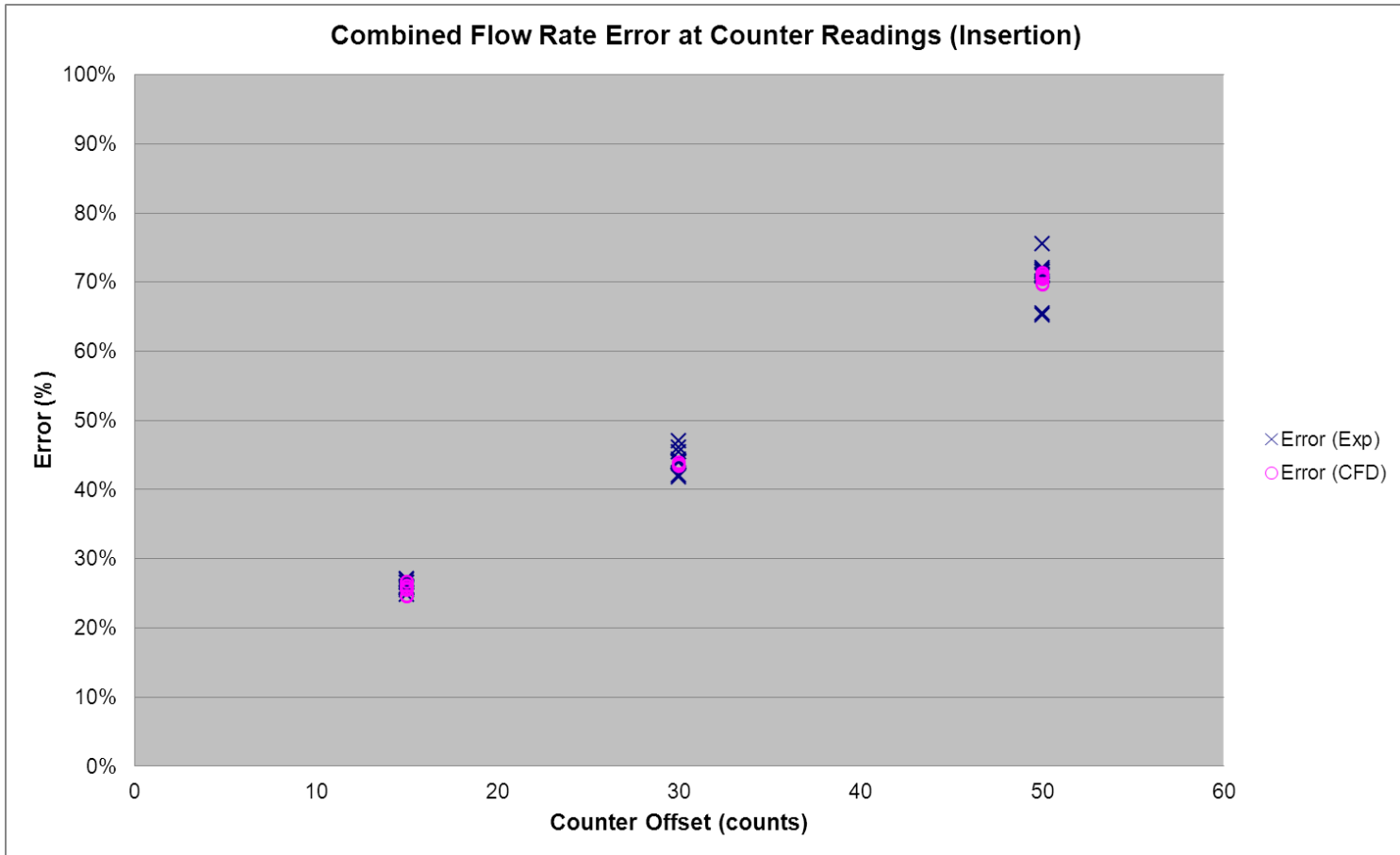
Results - CFD



Results - Experimental



Results - Combined



Results - Combined

Counter Reading	Experimental Error (%)		CFD Error (%)		Difference in Mean (% relative)
	Mean	Std. Dev.	Mean	Std. Dev.	
99985	26.1 %	0.7 %	25.7 %	0.7 %	-1.4 %
99950	70.6 %	3.1 %	70.6 %	0.6 %	0.0 %

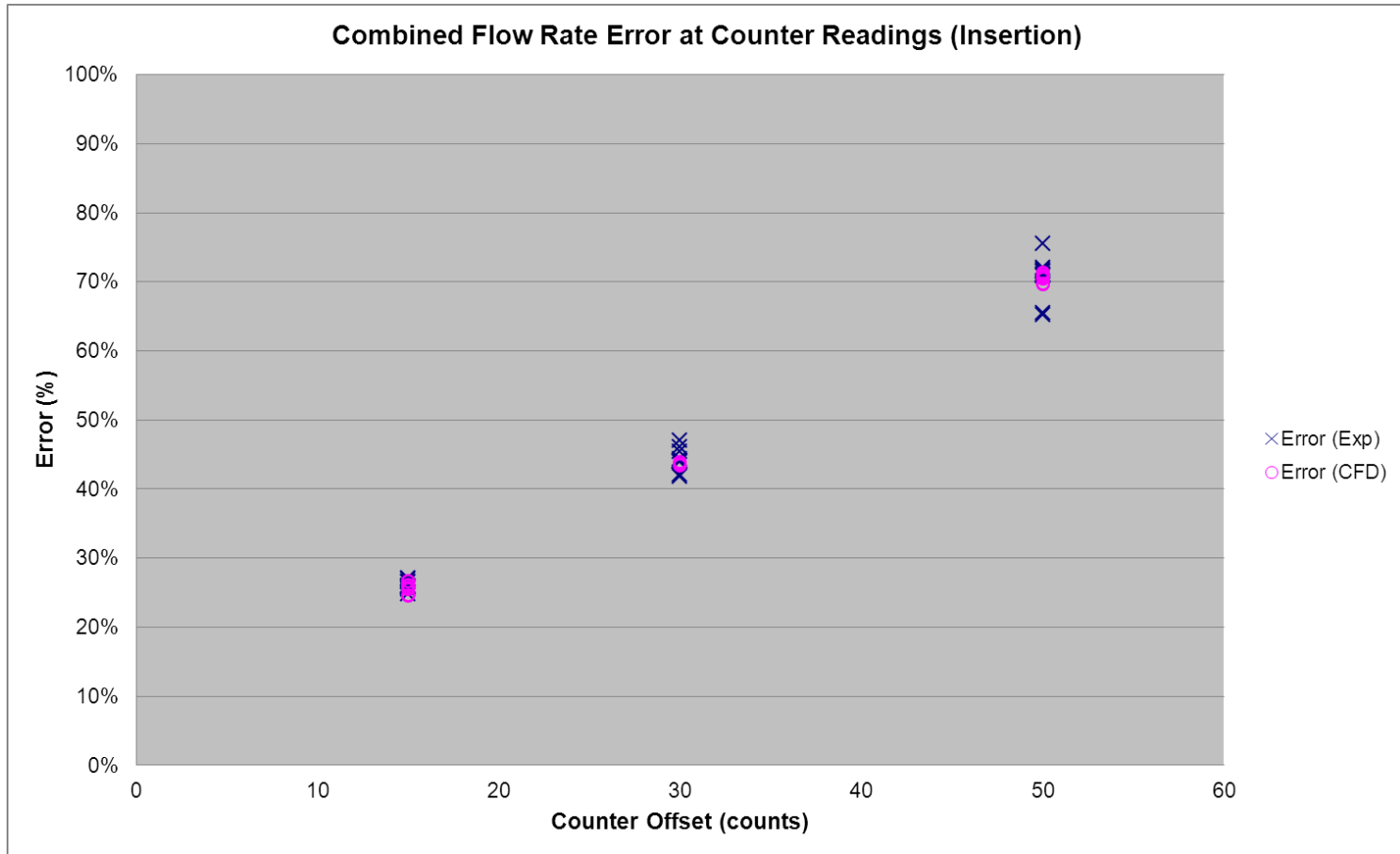
- High standard deviations at low DPs
 - Expected with higher uncertainty of DP measurement

Results - Combined

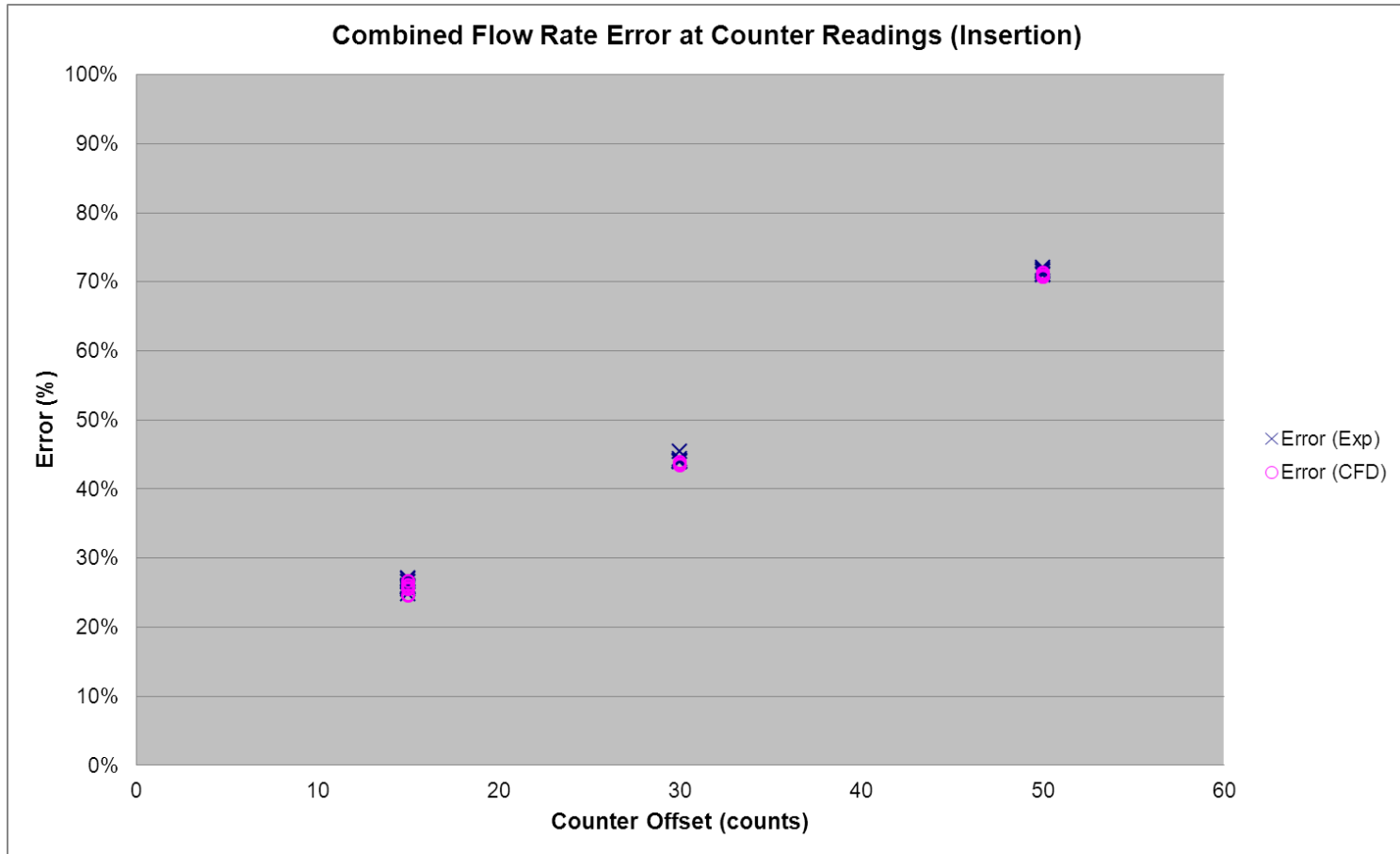
Counter Reading	Experimental Error (%)		CFD Error (%)		Difference in Mean (% relative)
	Mean	Std. Dev.	Mean	Std. Dev.	
99950 (All)	70.6 %	3.1 %	70.6 %	0.6 %	0.0 %
99950 (>10 mbar)	71.5 %	0.4 %	71.0 %	0.3 %	-0.7 %

- Excluding DPs below 10 mbar significantly reduces standard deviation
 - Demonstrates that the two data sets are more reliable above 10 mbar

Results - Combined



Results - Combined



Summary of First Error Period

- 21st July 2009 to 27th July 2010
- Counter reading of 99985 based on
 - ~31% step change in flow rate when the plate was inserted
 - 99885 values stamped on the carrier information plate
 - Pattern of contamination compared to physical measurements
- Mean error from on-site testing is 26.1 % (under-registration)
 - Standard deviation of 0.7 %
 - Supported by CFD (Mean 25.7 %; Standard deviation 0.7 %)
- Error is independent of process conditions
 - Single correction factor for period (1.353066)

Summary of Second Error Period

- 27th July 2010 to 10th August 2010
- Counter reading of 99950 based on
 - ~69% step change in flow rate when the plate location was corrected
 - 9995 value stamped on the carrier information plate
 - Interviews with mechanical operatives
- Mean error from on-site testing is 71.5 % (under-registration)
 - Standard deviation of 0.4 %
 - Supported by CFD (Mean 71.0 %; Standard deviation 0.3 %)
- Error is independent of process conditions
 - Single correction factor for period (3.506731)

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Thank you. Any Questions?

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