

Stage 02: Combined Workgroup Report

0498:

Amendment to Gas Quality NTS Entry Specification at BP Teesside System Entry Point

0502:

Amendment to Gas Quality NTS Entry Specification at the px Teesside System Entry Point

0498: This modification will facilitate a change to the current contractual Carbon Dioxide limit at the BP Teesside System Entry Point, through modification of a Network Entry Provision contained within the Network Entry Agreement (NEA) between National Grid plc and Amoco (UK) Exploration Company LLC in respect of the CATS Terminal (BP Teesside).

0502: This modification will facilitate a change to the current contractual Carbon Dioxide limit at the px Teesside System Entry Point, through modification of a Network Entry Provision contained within the Network Entry Agreement (NEA) between National Grid Gas and px (TGPP) Limited in respect of the px Teesside System Entry Point.

Since these modifications are identical in nature, differing only in the impacted NEA, the Modification Panel requested a single report encompassing both. For simplicity, information in this report has been presented once but applies equally to both 0498 and 0502.



The Workgroup recommends that these modifications should now proceed to consultation.



Medium Impact: Transporters, Shippers and Consumers

At what stage is this document in the process?









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Transporter:

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Systems Provider: **Xoserve**



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About this document:

This combined report will be presented to the Panel on 21 May 2015.

The Panel will consider whether these modifications should proceed to consultation or be returned to the Workgroup for further assessment.

The Workgroup recommends the following timetable	e:
Initial consideration by Workgroup	01 May 2014
Amended Modification considered by Workgroup	n/a
Workgroup Report presented to Panel	21 May 2015
Draft Modification Report issued for Consultation	21 May 2015
Consultation Close-out for representations	11 June 2015
Final Modification Report published for Panel	12 June 2015
UNC Modification Panel decision	18 June 2015

1 Summary

Are these Self-Governance Modifications?

The Modification Panel determined that these are not self-governance modifications because they are likely to have an impact on Shippers, Transporters or consumers of gas conveyed through pipes.

Why Change?

0498 - The current carbon dioxide limit at BP Teesside System Entry Point of 2.9 mol% is incompatible with the anticipated gas quality specification of some potential new offshore developments. While the inclusion of processing and treatment solutions to remove the excess carbon dioxide are being considered upstream of the National Transmission System (NTS), these would require significant investment and/or operating costs, reducing the economic delivery of those developments. Hence, this modification seeks to establish whether a change of one of the existing Network Entry Agreement (NEA) parameters would be a more efficient and economic approach to facilitate delivery of potential new supplies to the System, subject to ensuring no adverse impact on consumers or on the operation of the pipeline system.

0502 - The px Delivery Facility receives the same composition of commingled gas from the Central Area Transmission System (CATS) pipeline as the BP CATS Facility, and currently has the same carbon dioxide limit within its Network Entry Provisions.

Solution

Both modifications propose an amendment to a Network Entry Provision, to permit an increase in the CO₂ limit of gas delivered from the respective Entry Points into the NTS.

0498 - This modification, in accordance with UNC TPD I 2.2.3(a), proposes an amendment to a Network Entry Provision within the existing NEA in respect of BP Teesside System Entry Point. This amendment would increase the CO_2 limit of gas delivered from the BP Teesside System Entry Point into the National Transmission System to 4.0 mol% from the current limit of 2.9 mol%.

0502 - This modification, in accordance with UNC TPD I 2.2.3(a), proposes an amendment to a Network Entry Provision within the existing NEA in respect of the px Teesside System Entry Point. This amendment would increase the CO₂ limit of gas delivered from the px Teesside System Entry Point into the NTS to 4.0 mol% from the current limit of 2.9 mol%.

Relevant Objectives

For both Modifications **0498** and **0502** it is believed that the increase to a higher CO₂ limit will permit economic delivery of additional UK Continental Shelf (UKCS) gas production, increasing GB supply security and reducing reliance on imported gas. This will contribute to the economic and efficient operation of the total system through maintaining a diversified supply base and by continued use of existing capacity.

It will provide greater competition between Shippers and between Suppliers by increasing gas availability in the market and also securing greater supply for consumers.

Implementation costs

No significant implementation costs have been identified with changing the Gas Entry Conditions in respect of BP Teesside System Entry Point or of px Teesside System Entry Point.

Implementation

The Workgroup has not proposed a timescale for implementation of these modifications, but would suggest that they are implemented simultaneously at the earliest practical opportunity.

Does this modification impact a Significant Code Review (SCR) or other significant industry change projects, if so, how?

This does not affect the UK Link Replacement Programme delivery or any other change.

2 Why Change?

0498 - With the increasing maturity of the UKCS as a gas production area, the accessibility of new fields and improved extractability from existing fields increase in importance to the UK. Some current production relies on blending with other fields in order to meet Gas Entry Conditions, and other potential new upstream developments are known to have CO₂ levels that exceed current limits. The current CO₂ limit at Teesside already causes curtailments to production on certain days when insufficient blending gas is available and the current limit would be temporarily exceeded. In addition, by analysing the CO₂ content of future gas production potentially entering the System at Teesside, BP has identified an increasing risk that, especially in summer months and from 2019 onwards, the availability of sufficient blending gas cannot be guaranteed prior to entry into the NTS.

Under the prospect of reduced blending opportunities there would be an increasing risk of interruption of gas flows, which would affect gas production processes. This problem could be addressed by treating the gas for removal of CO₂ at the wellhead or at the terminal, but the investment to bring the quality in line with current specification would be significant, thus increasing materially the risk of making some upstream projects, currently being evaluated, less economic.

To assess the feasibility of a higher CO₂ content, BP has undertaken an analysis of the potential impacts and has engaged with National Grid NTS to understand whether a higher limit would be compatible with network safety and operational efficiency. The preliminary results of National Grid NTS and BP work have so far identified no material increase in risks in the NTS associated with 4.0 mol% carbon dioxide content. In addition, as there are some legacy arrangements in place granting a similar limit at some NTS Entry Points, it seems plausible that gas with higher CO₂ content could be potentially accommodated without impacting NTS integrity and/or consumers and/or cross border trade. It should also be noted that CO2 is not a defined parameter in the Gas Safety (Management) Regulations 1996, and no amendment of GSMR is reguired.

Similar arguments for change have been put forward under Modification 0502.

0502 - The px Delivery Facility receives the same commingled gas from the CATS pipeline as the BP CATS Facility, and therefore any changes to the commingled gas composition that may affect BP's processing ability, would have the same impact upon the px Delivery Facility. If Modification 0498 is approved and the specification in the pipeline changes as predicted by BP, then without this equivalent Modification 0502 to change the carbon dioxide limit at the px Teesside System Entry Point to align with BP, there is a risk that

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deliveries from the px Teesside System Entry Point will be curtailed when the CATS pipeline specification reaches the current CO₂ limit, resulting in the interruption of gas flows into the NTS.

Industry engagement was sought, through this combined Workgroup, to assess more thoroughly the impact of the proposed changes under these modifications, in order to establish whether a higher CO₂ limit at the px Teesside System Entry Point, alongside the same higher limit proposed at the BP Teesside System Entry Point, would be beneficial for the GB market.

3 Solution

UNC (TPD Ref I 2.2.3(a)) states the following:

"2.2.3 Where

(a) the Transporter and the relevant Delivery Facility Operator have agreed (subject to a Code Modification) upon an amendment to any such Network Entry Provisions, such Network Entry Provisions may be amended for the purposes of the Code by way of Code Modification pursuant to the Modification Rules"

Modification 0498

This modification seeks to amend a Network Entry Provision within the existing BP Teesside NEA. This amendment would increase the CO₂ upper limit for gas delivered from the BP Teesside System Entry Point into the NTS to 4.0 mol% from the current limit of 2.9 mol%.

Modification 0502

This modification seeks to amend the Network Entry Provision within the existing px (TGPP) Limited NEA. This amendment would increase the CO₂ upper limit for gas delivered from the px Teesside System Entry Point into the NTS to 4.0 mol% from the current limit of 2.9 mol%.

User Pays

Classification of these modifications as User Pays, or not, and the justification for such classification.

No User Pays service would be created or amended by implementation of either of these modifications and they are not, therefore, classified as User Pays Modifications.

Identification of Users of the service, the proposed split of the recovery between Gas Transporters and Users for User Pays costs and the justification for such view.

None

Proposed charge(s) for application of User Pays charges to Shippers.

None

Proposed charge for inclusion in the Agency Charging Statement (ACS) – to be completed upon receipt of a cost estimate from Xoserve.

None

4 Relevant Objectives

lm	pact of the modifications on the Relevant Objectives:	
Re	elevant Objective	Identified impact
a)	Efficient and economic operation of the pipe-line system.	0498 and 0502 : Impacted
b)	Coordinated, efficient and economic operation of (i) the combined pipe-line system, and/ or (ii) the pipe-line system of one or more other relevant gas transporters.	0498 and 0502 : Impacted
c)	Efficient discharge of the licensee's obligations.	None
d)	Securing of effective competition: (i) between relevant shippers; (ii) between relevant suppliers; and/or (iii) between DN operators (who have entered into transportation arrangements with other relevant gas transporters) and relevant shippers.	0498 and 0502 : Impacted
e)	Provision of reasonable economic incentives for relevant suppliers to secure that the domestic customer supply security standards are satisfied as respects the availability of gas to their domestic customers.	0498 and 0502 : Impacted
f)	Promotion of efficiency in the implementation and administration of the Code.	None
g)	Compliance with the Regulation and any relevant legally binding decisions of the European Commission and/or the Agency for the Co-operation of Energy Regulators.	None

Impact on Relevant Objectives (whole section to be considered and confirmed)

The Workgroup concluded that there were impacts to four Relevant Objectives:

- a) Efficient and economic operation of the pipe-line system
- b) Coordinated, efficient operation of the offshore and onshore systems
- d) Competition between relevant shippers
- e) Incentives to provide gas for domestic customers in line with supply security standard.

Views differed between participants and no clear consensus was reached. In the following pages these views are explained further.

Initial Representations

Initial representations were received from SSE, GrowHow and Tata Steel and are published alongside this report and views from Scotia Gas Networks were included in the minutes of 03 July 2014 Workgroup meeting (available here).

Issues raised in these representations include:

- Our CO₂ emissions increase as the additional CO₂ is emitted from our process in addition to the CO₂ we
 are generating ourselves (this would presumably take the form of an increased emissions factor on the
 metered incoming gas), leading to higher costs under EU ETS.
- There would be additional load on our CO₂ removal systems, which are already highly loaded at maximum production rates so this could become a limit on production rate.
- Calorific value is reduced, so our volume of gas consumed needs to increase, this will increase pressure
 drop in the distribution pipework (both NG system and customers own distribution system).
- The CO₂ acts a diluent, so where we are trying to achieve high temperatures (e.g. in reformer furnaces) we have more mass to heat, which consumes more energy (minor effect).
- If the added CO₂ displaces a 'high' hydrocarbon the effect on these will be different to the displacement of a 'low' hydrocarbon. A quick calculation suggests that the move from 2.9% to 4%, with a reduction in methane (CH₄), will reduce the CV by about 1% and the Wobbe by 2%.
- Gas turbine combustion dynamics, emissions and operability are impacted by the total level of inerts (principally CO₂ and Nitrogen) contained in the gas. Certain gas turbine Original Equipment Manufacturers (OEMs) stipulate a maximum level of 4% inerts in their fuel gas specifications, operation outside this specification could invalidate the unit's warranty or service agreement. As a result this will prevent operation of the asset and result in lost revenue and less competition in the market for supplying electricity. Where new build is being considered, an increase in CO₂ to 4.0 mol% could restrict the selection of which future gas turbine manufacturer could be used, suppressing market competition.
- Increasing the level of inerts creates the potential for a greater range of gas composition and specification. Varying gas specification within this wider range will lead to a requirement for unpredictable gas turbine re-tuning in order to maintain combustion stability and dynamics within the OEM's specification to avoid warranty and Environment Agency breaches. Currently, re-tuning of gas turbine combustion systems takes around 4 hours, is costly as it requires the services of specialist OEM combustion engineers to retune the combustion system and prevents flexible, load following operation during that period. This lack of flexibility will not only impact on being able to support intermittent generation and security of supply but lead to loss of revenue, the magnitude of which will be dependent upon when the gas composition changes. In addition changes in Gas Quality could result in gas turbine start up and transfer issues. This represents a real risk to the reliability of future operations especially for stations operating in a cyclic mode with implications for providing support for intermittent generation and hence electricity system security.
- The proposed increase in CO₂ of the gas composition will increase the amount of CO₂ released to the
 atmosphere and will lead to additional costs for gas turbine operators because they will have to pay for
 the increase in inherent CO₂ through EU ETS liabilities.

The Workgroup considered these issues as part of their overall assessment.

WORKGROUP ASSESSMENT

The Workgroup identified the issues raised by these modifications and collated them into a number of key themes, as follows:

- Further Background to the Change
- Anticipated Impact on Gas Quality
- National Grid NTS' Assessment of their Operational Risks
- Impact on Consumers
- Impact on Storage Operators
- Carbon Cost Assessment
- Other Implications of Not Changing the NEA
- Wider Considerations
- Conclusions

Further Background to the Change

BP and TGPP consider that the current specification for CO₂ at the Teesside entry points is incompatible with the composition of some natural gas from potential upstream developments. BP has observed the current CO₂ limit is already causing interruption to existing production on certain days. At least one future development in the Central North Sea area defined by the CATS catchment area would benefit from an increase in the NTS entry specification at Teesside from 2.8 mol% to 4.0 mol%. Studies are currently underway to determine the optimal development plan for the Jackdaw development. The Jackdaw discovery was made in 2005 and is one of a number of significant gas discoveries in the area. Operated by BG plc, the discovery is located in the ultra-High Pressure High Temperature (uHPHT) province of the Central North Sea. Given the uHPHT nature of the reservoir development costs are high (estimated to be in the region of £3bn). Timing of first gas for the development is expected to be in the late teens or early 2020s. The significant size of the find will help underpin UK energy supply over twenty years but the high cost associated with uHPHT developments makes the developing this and other discoveries challenging. It is essential that the initial capital cost is kept as low as possible. The requirement to remove CO₂ from the Jackdaw gas would add significantly to the development cost.

The CATS and TGPP Network Entry Agreements (NEAs) already have Reasonable Endeavours rights (what are the impacts of this in practice?) for short-term breaches of CO₂ up to a maximum of 4.0 mol% while other UK terminals currently have a 4.0 mol% NTS entry specification. Increasing the current CO₂ specification at the Teesside entry points to 4 mol% would result in more efficient utilization of existing infrastructure capacity, extend the useful life of existing assets and contribute significantly (?) to Maximisation of Economic Recovery of oil and gas from the UK continental shelf (MERUK).

Simplified Technical Explanation of impact of increasing CO_2 on Gas Quality at Teesside CATS and TGPP adhere strictly to all NEA specifications which includes: Wobbe >48.14 <51.41; ICF <0.48; SI <0.60.

An assessment of the impact of CO₂ content on Calorific Value (CV), Wobbe Index (WI), Soot Index (SI) and Incomplete Combustion Factor (ICF) has been carried out by BP. The assessment is based on daily average flows between 01 January 2013 and 07 July 2014 and correlates CO₂ content of the NTS delivery gas to the parameter noted above. The findings were presented by BP at the Workgroup meeting on 07 August 2014 (available here). The analysis shows that gas delivered into the NTS from the Teesside entry points will

remain well within current NTS specification limits for GCV, Wobbe, ICF and SI even at the maximum requested CO₂ limit of 4.0 mol%. Detailed analysis can be found in Appendix 2.

Forecast Levels of CO₂ in gas at Teesside

The average CO₂ content of gas entering the NTS at the px Teesside entry point over the last two years has been 2.18 mol%. Currently, there are occasional days when CO₂ content exceeds the current specification limit and post 2019, there is the potential for development of at least one new field in the CATS catchment containing elevated levels of CO₂ in the produced gas. Analysis by BP and TGPP of forecast future gas production from offshore fields has shown that for the majority of time, the CO₂ content of gas entering the NTS at the Teesside entry points is likely to be similar to historic norms and well below the current 2.9 mol% specification limit. This is achieved through the blending of gas with high CO₂ content with gas low in CO₂ from other fields feeding into the CATS pipeline and being exported in the pipeline as commingled flow. Issues may arise however, when fields are shutdown during summer maintenance periods or during unplanned production upsets at offshore fields when flows of gas in the CATS pipeline are reduced and there is insufficient gas low in CO₂ to blend the high CO₂ gas into specification.

Up to 2018 CO₂ levels could exceed 2.9 mol% for short periods (c.2-3 days) during summer maintenance periods. As a result, the overall annual average impact is forecast to be 0.03 mol%.

From 2019 onwards, CO_2 levels in CATS/TGPP export gas during the summer months are likely to range between 2.66 mol% and 3.6 mol% (max 4.0 mol%) with CO_2 levels in non-summer months ranging between 2.66 mol% and 3.0 mol% (max 3.57 mol%). It is important to stress that elevated CO_2 levels are not anticipated to be the norm and CO_2 levels in excess of 2.9 mol% are only expected to occur for short durations.

Anticipated Impact on Gas Quality

National Grid NTS' Assessment of their Operational Risks

National Grid NTS has completed an exercise, supported by network analysis, to assess the possible NTS operational risks arising from higher CO₂ levels. National Grid NTS has assessed the risks (which are discussed further below) in terms of:

- Safety
- Operations
- Contractual obligations and cross border flows
- · Potential for impacts on parties downstream of the NTS

Safety

There is no prescribed regulatory limit for CO_2 in GB, and parts of the NTS (e.g. two of the St Fergus subterminals) have had 4 mol% legacy contractual CO_2 limits for many years with no known evidence of additional corrosion (as expected from the "dry gas" NTS system). CO_2 levels in the NTS in Scotland are typically higher than in southern parts of the network e.g. September 2013 to August 2014 – average from St Fergus ASEP of 2.0% CO_2 , compared to average 1.1% CO_2 in Norfolk.

DRa to provide evidence of flows at [St. Fergus] to demonstrate (or not) that the NTS has experienced gas at 4mol% CO2?? – Further Appendix for St. Fergus trend chart and a table of other Entry Points showing average and range of CO2

Operations

This is similar to safety in terms of engineering operation. Commercially the lower CV expected from higher CO_2 gas has been assessed with CV shrinkage modelling and was shown to be not material by NTS. Impact on CO_2 emissions from NTS' gas fired compressors is likely to be small and not material in the context of all the other variables that affect this.

Contractual obligations and cross border flows

There are currently no regulatory CO₂ limits at cross border points. Whilst the Workgroup did discuss EU initiatives on gas quality harmonisation it also recognised that there are no gas quality limits (including CO₂) in the EU legislative development process. Insert info on the CEN study – taken from the EU WG (Phil H)

- IUK has an entry condition (exit from NTS) of 2.5% CO₂ (driven by Belgian limits¹) but otherwise there are no CO₂ contractual obligations at NTS offtakes. Network analysis based on the range of scenarios indicated in the 2013 Gas Ten Year Statement (derived from Future Energy Scenarios) shows that gas from Teesside would expect to be little or no proportion of the flow offtaken at Bacton (IUK).
- Offtake of gas at Moffat to Ireland is in a part of the NTS that has had higher legacy CO₂ limits (than for Teesside) for more than a decade. Again Teesside gas would not typically be expected to be a substantial part of the flow at Moffat.

Potential for Impacts to parties downstream of the NTS Pre-Engagement??

Prior to these modification proposals being published National Grid NTS wrote out inviting comments from potentially impacted parties. National Grid NTS received 9 responses provided on a private basis and all² substantive points have since been discussed in the Workgroup. National Grid NTS's network analysis also enabled publication via this Workgroup of maps (high demand and low demand) showing where Teesside gas is modelled to make up a proportion of 25% or more of the flow at NTS offtakes. These maps are shown in Appendix 1.

During the course of the development phase National Grid NTS has written out again encouraging potentially impacted parties to bring their views to this Workgroup.

Impact on consumers

Combined Cycle Gas Turbines (CCGTs) can only tolerate limited changes in gas composition (referenced as WI and/or Heating Value), dependent on the OEM (Original Equipment Manufacturer) and control systems. Each CCGT must be tuned to operate in a particular narrow band of gas composition to maximise efficiency and remain within environmental emissions limits.

The proposed increase to the level of inerts creates the potential for a greater range of gas composition. Within this wider range, the potential then exists for larger fuel composition variation. This can have a negative impact on CCGT operation despite the gas being within that range allowed by the Gas Safety (Management) Regulations (GSMR) and OEM specifications. Varying gas specification within this wider range will lead to a requirement for unpredictable gas turbine re-tuning in order to maintain combustion stability and dynamics to avoid Environment Agency breaches. If this is not possible the plant will trip to be protected from further damage, although the trip event is undesirable due to asset life reduction, loss of revenue, cash out and penalty regimes (more information to explain these). The sensitivity of CCGTs to gas

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quality is more fully described in the document shared with the Workgroup on (extracts from the doc, recognising the technical complexity?):

http://www.gasgovernance.co.uk/sites/default/files/Impact of Natural Gas Composition - Paper 0.pdf

Currently, re-tuning of gas turbine combustion systems takes around 4 hours, it is costly as it requires the services of specialist OEM combustion engineers to retune the combustion system and prevents flexible, load following operation during that period. This lack of flexibility will not only impact on being able to support intermittent generation and subsequent security of supply but lead to loss of revenue, the magnitude of which will be dependent upon when the gas composition changes.

A number of examples have been provided of times when plant has tripped. The Workgroup will investigate the cause of the trips, which is suspected to be a result of a change in gas quality (see Action 0807).

The proposed increase in CO_2 of the gas composition will increase the amount of CO_2 released to the atmosphere and will lead to additional costs for gas turbine operators because they will have to pay for the increase in inherent CO_2 through EU ETS liabilities.³ An estimate of this is included in the Carbon Cost Assessment.

Safety related - no safety issues for consumers?

Shipper identified...commercial and contractual issues – to be considered by shipper participants (potential trip leading to Elec Capacity Mechanism Impacts)

Consumer identified.....Energy UK

Do DNs have any CO2 obligations – or is this included in the CCA? Offtake Arrangements Doc? Energy Efficiency Directive?

Small supply point impacts – explanation of how FWACV mitigates the impact

Also consider the impact on flame stability (JCh?)

Is there a competitive disadvantage for consumers close to Teesside?

Impact on Storage Operators (AMi to work on quantifying impacts and costs)

The principal concern for Gas Storage Operators Group (GSOG) members relates to increases in the absolute levels of CO_2 in gas on the NTS, rather than speed of gas quality change, because of the increased risk of corrosion from higher CO_2 gas. This risk arises because higher CO_2 results in higher carbonic acid levels in the aqueous condensate. Increased carbonic acid increases the rate of corrosion in the underground pipework.

The cost impact on storage operators is difficult to predict given the information provided in the development of these modifications. However, should the changes at Teesside result in higher levels of CO₂ particularly for extended periods during the summer when storage sites are often injecting gas from the NTS, storage operators will need to increase corrosion monitoring and mitigation activities. The level of CO₂ will depend to some degree on the particular site, however members have noted that sustained levels of gas with greater than 1.7 mol% CO₂ will require them to reassess of their carbonic acid monitoring and treatment programme. Others have noted that the 2.5 mol% level could create significant challenges for storage systems.

In addition to the risk associated with carbonic acid, increasing the CO_2 of gas also results in higher costs for storage operators because it means that higher volumes of gas needs to be injected into storage facilities in order to inject the same calorific value of the gas. This means that the storage operators will need to use

³ http://ec.europa.eu/clima/policies/ets/monitoring/docs/gd1_guidance_installations_en.pdf (p80/81)

more energy to get gas into and out of sto ETS permits.	ore. The increased use o	of fuel to move the gas will r	equire more EU

Carbon Cost Assessment

Options Considered (Expand the options to include 1. Consideration of Field Development with restricted flow, 2. Not developed at all – other sources take up the demand, 3. field development with treatment of some kind – these 3 options)

The options for addressing the possible increases in CO_2 levels in export gas are to either allow such gas to flow directly into the NTS up to an agreed level (4.0 mol%) or to remove the excess CO2 above the current allowable specification using CO_2 removal technology. The CO_2 emissions and associated cost of such emissions are estimated in the Carbon Cost Assessment (see below).

Option 1 - Flow gas up to 4.0 mol% CO2 into the NTS

As noted above, flowing gas in excess of the current spec of 2.9 mol% is not expected to be for extended periods of time as it is anticipated that under normal operating conditions gas from any fields with gas of high CO_2 content would be blended in the offshore pipeline to ensure current delivery specifications are met. High CO_2 gas could result from maintenance of offshore fields during summer months or unplanned field operational outages when flows of gas into the CATS pipeline could be reduced and the capacity to blend high CO_2 gas reduced. The advantages to the upstream producers and the gas terminal operators is the removal of the need for significant capital expenditure and increased operating cost from the installation of CO_2 removal equipment which may be used for only a few days/weeks per year. This option would also prevent significant additional CO_2 being released to atmosphere from the use of process heat associated with the CO_2 removal technology.

Removal of CO₂ above 2.9 mol% at the upstream platform or at the terminals

There are a number of technologies available for removal of CO₂ from natural gas. The most suitable technology for a particular application depends on factors such as removal duty, inlet/outlet CO₂ concentrations, contaminants, operating conditions, volumetric flow, downstream processing requirements and relative capital / operating costs.

Based upon likely CO_2 & Hydrogen Sulphide (H_2S) partial pressures in the raw gas at the terminal and the required NTS entry specification, the most suitable technology to achieve a reduction in CO_2 from 4 mol% to 2.9 mol% for gas delivered to the Teesside entry point is a Formulated Amine Process.

The Formulated Amine Process consists of an absorber column and regeneration unit. Amine solution flows against the gas stream in an absorber column. CO_2 is absorbed producing a sweetened gas stream and CO_2 rich amine solution. Rich amine is routed to the regeneration unit where it is flashed to low pressure and heated producing a CO_2 stream for venting and lean solvent routed back to the absorber. Apart from capital cost, significant heat input is required to regenerate the amine and also to regenerate the TEG/MEG used to dehydrate the gas after passing through the amine unit. Heat is usually supplied by a hot oil system heated by natural gas - this generates further CO_2 emissions in addition to the CO_2 extracted from the natural gas. Electrical power is required to drive pumps and control systems.

Option 2 - Installation of an amine unit on the offshore facility

In order to ensure that discoveries such as Jackdaw can be economically developed, it is essential that capital costs be minimised. The fully installed cost of an offshore amine unit is likely to be in the order of £180m, which would be borne by the field owners.

The provision of an amine unit on a facility such as Jackdaw would allow the export of gas into the CATS pipeline that meets the CATS pipeline gas delivery specification for CO₂ at less than 2.8 mol%. As a result, it is likely that the CO₂ content of gas exported into the NTS from the Px Teesside and CATS entry points would remain unchanged from the current ranges observed.

It is possible that the requirement to provide an amine unit for removal of CO₂ on a facility such as Jackdaw could make the development project sub-economic for the field owners and development could be either delayed or postponed.

Option 3 - Installation of amine unit(s) onshore at the TGPP and CATS Facilities

If CO_2 removal facilities were not installed offshore, then in order to ensure that CO_2 levels remain within the NTS entry specifications it would be necessary to install an amine unit or units at the terminals. CO_2 removal facilities would need to be installed at the lower pressure (c. 65 bar) exit points of the terminals as the pipeline and terminal entry points operate at high pressure (c. 105 bar). The cost of installation of an amine unit at a Teesside processing facility is c. £200m (inconsistent with the table, appears in 3 places). The additional cost over an offshore unit is due to the requirement to process larger volumes of gas from the commingled pipeline stream.

At present the NTS entry points at Teesside are separate (px Teesside and CATS) and governed by separate Network Entry Agreements. Contractually the flow of gas from both the Px Teesside and CATS entry points are required to remain within the NTS entry specifications defined in the NEAs. Currently therefore, two amine units would be required (are the figures in the tables reflective of 1 or 2 units?) to ensure that contractual obligations are maintained and the cost of provision of these units would be borne by the offshore producers requiring use of the service. However, it will be difficult to force an upstream user processing gas in either TGPP or the CATS plant to pay for CO₂ removal facilities in the other plant where the producer is not processing gas and no contractual relationship exists.

A more efficient approach would be the installation of single amine unit at one plant with costs and blending rights agreed between TGPP, CATS and the upstream parties and the appropriate NTS entry specifications agreed between TGPP, CATS and NGG. At present however, with separate NEAs both flows are required to be on specification to the NTS.

It is anticipated that the amine unit (or units) would only be operated during those periods when the CO_2 content of the gas exported from the terminals exceeded 2.9 mol%. This allows process emissions resulting from operation of the unit(s) to be reduced. However, these cannot be reduced to zero as there is a requirement to maintain the amine tank at about 20° C when the fluid is not in use, which BP and TGPP estimate requires about 3.6MW of process heat.

Environmental impacts

Schematic (Appendix 4 prepared) and explanation of what/how (TGPP/BP)

CO ₂ Option	Cost (£MM)	Advantages	Disadvantages
Option 1 Flow gas at 4 Mol% CO ₂ into NTS	No equipment cost	 Low cost High CO₂ gas blended with other CATS gas for most of year Flow of high CO₂ gas for limited periods (Field maintenance, unplanned outages) Lower CO₂ emissions overall – no CO₂ released from process heat 	 Some high CO₂ content gas enters NTS on occasional days Slightly elevated emissions charges for consumers
Option 2 CO ₂ Removal Offshore at source		 Removes to CO₂ from specific high CO₂ gas Allows CATS pipeline gas to remain within current specification CO₂ content of NTS gas remains within current specification 	 Additional cost to specific project Additional CO₂ emissions from the use of process heat in addition to that removed from the gas Increased emissions charges Additional cost may make specific project sub-economic at assumed commodity prices Specific project delayed or not developed Ultimate recovery of oil and gas from UKCS is impacted
Option 3 CO ₂ Removal Onshore at terminal(s)		 High CO₂ content gas can be blended with low CO₂ content gas in the CATS pipeline Most of year CO₂ content of NTS gas remains within current specification without specific action CO₂ removal equipment provides backstop if CO₂ current CO₂ specification is exceeded 	 Operational pressure of CATS pipeline requires CO₂ removal equipment to be installed after gas is processed, prior to gas entering NTS Significant cost for provision of CO₂ removal equipment - Current NEA structure and separation of Teesside entry points may require 2 amine units (for CATS & TGPP) Equipment only operational for short duration Significant additional CO₂ released through process heat when operational and requirement to ensure amine maintained at 20°C when not in use Significantly increased emissions charges Additional cost may make specific project sub-economic at assumed commodity prices Specific project delayed or not developed Ultimate recovery of oil and gas from UKCS is impacted

Carbon Cost (explain the basis)

The detailed carbon cost assessment and assumptions are included in Appendix 3. A carbon cost assessment has been calculated for each of the CO₂ options:

- Scenario 1 Non-removal of CO₂;
- Scenario 2 Removal Offshore; and,
- Scenario 3 Removal Onshore.

The assessment has been made for the period 2019 to 2030, 2019 being the earliest a field such as Jackdaw might be anticipated to start. For Scenarios 2 and 3, it is recognised (as noted above) that for the majority of time the CO_2 levels are likely to be below the current limit with CO_2 content above 2.9 mol% being possible during summer maintenance campaigns or for short periods of unplanned outages when gas with high CO_2 content cannot be blended in the CATS pipeline with gas with low CO_2 content. For the purposes of modelling the CO_2 impact assessment, this period has been assumed to be 30 days per year and the CO_2 content has been assumed to be a maximum of 4.0 mol% for this period. In reality BP and TGPP would expect this to be a worst case scenario with fewer days per year and with days when the CO_2 content is significantly less than the maximum assumed 4.0 mol%.

A summary of the overall CO₂ impact assessment is provided in the table below:

Assessment of CO ₂ Impact from Teesside Gas (2019-2030)	Scenario 1 NTS Delivery at 4 mol % CO2	Scenario 2 Offshore CO2 Reduction	Scenario 3 Onshore CO2 Reduction
CO ₂ Removed by Amine unit (4 mol% to 2.9 mol%) (te)	0	476,875	66,243
CO ₂ in fuel gas consumed by Amine unit (te)	0	219,920	172,046
CO ₂ above 2.9 mol% emitted by consumers (te)	64,256	0	0
Total additional CO₂ emissions (te)	64,256	696,795	238,289

The removal of CO_2 offshore results in the greatest level of CO_2 emissions (697 kte) as there is a requirement to treat the entire gas stream being exported the production platform. Removing CO_2 above the current 2.9 mol% limit at the terminals results in lower CO_2 emissions (238 kte) than an offshore solution as gas with high levels of CO_2 is blended with low CO_2 gas for most of the time and treatment is only required for short periods. At 66 kte, removal of CO_2 from gas at the onshore terminal/terminals is comparable to but slightly higher than the CO_2 that would be emitted by consumers if such gas were delivered onto the NTS (64 kte) (the difference being due to the slight inefficiency of the amine system). While an amine unit at the terminal/terminals would remain non-operational for much of the year, there is a requirement to maintain the amine tank at about 20°C when the fluid is not in use. As a result, during the period of assessment, there is over 2.5 times more CO_2 released from process heat than is required to be removed from the gas to meet the current 2.9 mol% CO_2 limit for NTS gas. When this significant volume of CO_2 is considered, the overall level of CO_2 emissions remain significantly higher (238 kte in total) than allowing the gas to pass onto the NTS.

In terms of cost of abatement of the CO₂ generated above the current 2.9 mol% limit. These costs on an NPV10 basis (what is NPV10, and why is this appropriate?) are summarised in the table below:

Cost Assessment of CO₂ from Teesside Gas (2019-2030) (£ NVP10 1/1/15)	Scenario 1 NTS Delivery at 4 mol % CO2	Scenario 2 Offshore CO2 Reduction	Scenario 3 Onshore CO2 Reduction
CO ₂ Total ETS Traded Cost	£42,232	£1,741,921	£578,525
CO ₂ Total Traded Cost with Carbon Price Support	£269,723		
Total CO2 Cost (Traded & Price Support)	£311,954	£1,741,921	£578,525
CO ₂ Total Non-Traded Cost (£/yr) (non-ETS consumption)	£959,753	£0	£0
Total Estimated Emissions Cost	£1,271,707	£1,741,921	£578,525
Estimated Fully Installed Cost of Amine Unit		£147,189,400	£129,089,543
Estimated Abatement Cost for additional CO2 prior to NTS entry		£148,931,320	£129,668,068
Cost per tonne	£20	£214	£544

In terms of ETS traded costs where CO_2 emissions costs are measured against market prices, the highest cost option (NPV10 £1.7m) would be removal of CO_2 offshore as this option results in the largest volume of CO_2 emitted. The cost of removal of CO_2 onshore at the terminals is also significant (NPV10 £578k) due to the substantial amount of CO_2 emitted through process heat. Delivery of gas with 4.0 mol% CO_2 content onto the NTS is impacted by the requirement for power generators to pay substantially higher charges for emitted CO_2 due to the Carbon Price Support scheme. However at NPV10 £312k this is the lowest cost option given the forecast small number of days per year when such gas is being produced at the terminals.

If the impact of consumption of gas by non-ETS paying consumers is considered (using the DECC pricing assumption for Non Traded CO_2 emissions), the CO_2 emissions cost of NTS delivery of 4.0 mol% CO_2 gas increases significantly to c. £1.27m. However, it is felt that if the non-traded cost of CO_2 is taken into consideration then the capital cost of installing CO_2 mitigation should also be considered. While the capex figures used here are high level estimates and would be refined with further design work it is estimated that the fully installed cost of an amine unit on an offshore platform would be in the region of £130m and the cost of an onshore unit would be of the order of £147m (both discounted to 01 January 2015 at 10%).

Including the cost of the amine units brings the total NPV of mitigating the increased CO_2 – which may be in only excess of the current 2.9 mol% for 30 days per year and most likely less – to between £131m and £148m. This is over 100 times more costly than the £1.27m estimate if the CO_2 were delivered onto the NTS. In tonnage terms, the cost to an NTS gas consumer (needs definition) is c. £20/te but costs could be up to £500/te to mitigate the CO_2 prior to gas entering the NTS.

Wider Considerations

Context and value/cost for the UK

Predictions of composition of future gas supplies? Short term and long term views? Forward planning?

Risk of setting precedent – set out the argument / seek views from respondents??

Non-discrimination (DRa to provide NG opinion on why they aren't discriminating)

Policy explanation of Carbon reduction vs sustainable UKCS

TGPP/BP with MH support to consider and compile this section

Other Implications of Not Changing the NEAs

If not approved, what will the developers do?

Conclusions Views welcome

No clear conclusions have been achieved. Workgroup participants differed in their view of these changes, depending on the impacts they believed were most relevant to them. This report seeks only to document the arguments to inform further consideration within the UNC modification process (which assesses against the Relevant Objectives).

Participants believed that there are other considerations, such as the wider UK interest and UK Government Policy, which are beyond the vires of a UNC modification.

5 Implementation

The Workgroup has not proposed a timescale for implementation of these modifications, but would suggest that they are implemented [simultaneously] at the earliest practical opportunity.

6 Impacts

Does this modification impact a Significant Code Review (SCR) or other significant industry change projects, if so, how?

This does not affect the UK Link Replacement Programme delivery or any other change.

7 Legal Text

No changes to the UNC are proposed under either Modification 0498 or 0502.

Suggested text to modify the Network Entry Provisions contained within the relevant NEA has been provided by each Proposer.

No issues were raised by the Workgroup regarding either content.

Suggested Text - Modification 0498

Given the relative simplicity of the legal change, the following legal text is suggested to modify the Network Entry Provisions contained within the NEA.

2.3 Gas tendered for delivery by System Users to the System at the System Entry Point shall not contain any solid, liquid or gaseous material which would interfere with the integrity or operation of the System or any pipeline connected to

such System or any appliance which a consumer might reasonably be expected to have connected to the System. In addition, all gas delivered to the System at the System Entry Point shall be in accordance with the following values:

[...]

(k) Carbon Dioxide

Not More than 2.9% 4.0 mol%

Suggested Text - Modification 0502

The following legal text is suggested to modify the Network Entry Provisions contained within the NEA:

2.3 (k) Carbon Dioxide

not more than 2.9 4.0 mol%

8 Recommendation

The Workgroup invites the Panel to:

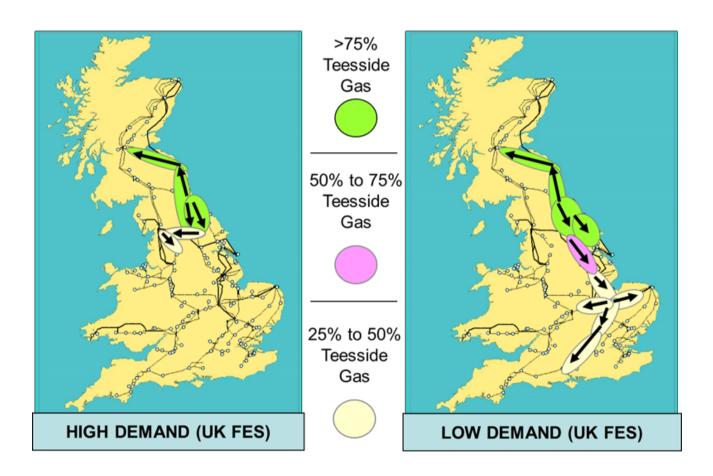
AGREE that these modifications should be submitted for consultation.

[?? Any additional questions for UNC Modification Panel consideration / potential inclusion in the consultation focus ???]

9 Appendices

- 1 Teesside Flow Maps
- 2 Detailed analysis of the impact of increasing CO₂ on Gas Quality at Teesside
- 3 CO₂ Impact Assessment
- 4 Teesside Schematics

Appendix 1 - Teesside Flow Maps





Appendix 3 - CO₂ Impact Assessment (new this version)

Summary

A carbon cost assessment has been calculated for the proposal (which?). The least impact on CO₂ emissions from bringing gas with up to 4.0 mol% CO₂ content into the CATS system is for such gas to be allowed to flow into the NTS. Significantly more CO₂ is emitted by removing CO₂ from the gas due to the need for process heat to remove CO₂. The cost of installing an amine unit either at specific fields offshore or at the onshore terminals is considerable. Current estimates for the fully installed cost of an offshore amine unit is of the order of £200m (undiscounted). When this is taken into account, the mitigation cost increases significantly when compared to the costs to NTS gas consumers (including non ETS participants). On a tonnage basis the cost to an NTS gas consumer (both ETS and Non-ETS participants) is c. £20/te but the cost to mitigate the higher levels of CO₂ prior to gas entering the NTS could be up to £500/te.

Introduction

A carbon cost assessment has been calculated for the proposal (which?). The impact assessment compares the tonnage of CO₂ released in order for the forecast gas landed at Teesside to meet the current 2.9 mol% CO₂ NTS entry specification and the cost of this CO₂ mitigation to the tonnages that would be released by downstream consumers if the Teesside NTS entry specification were to be raised to 4.0 mol% and such gas was not diluted by other NTS flows.

Three scenarios are therefore considered:

- Scenario 1 Non-removal of CO₂:
- Scenario 2 Reduction of CO₂ content to 2.9 mol% Offshore; and'
- Scenario 3 Reduction of CO₂ content to 2.9 mol% Onshore.

The assessment has been made for the period 2019 to 2030, 2019 being the earliest date that fields with elevated CO_2 content might be expected to come on stream. Where gas with an elevated CO_2 content flows into the CATS pipeline (Scenarios 1 and 3) this gas will be commingled with other gas with lower CO_2 content. As a result, it is expected that for the majority of time the CO_2 content of gas entering the Teesside NTS entry points is likely to be below the current limit. Increases above the current limit are most likely to be during summer maintenance campaigns or for short periods of unplanned outages when field outages means that gas flows at Teesside will be lower than normal and low CO_2 content gas for blending gas may be restricted. For the purposes of the CO_2 impact assessment, this period has been assumed to be 30 days per year and the CO_2 content has been assumed to be a maximum of 4.0 mol% for this period. In reality BP and TGPP would expect this to be a worst case scenario.

Assumptions

The assumptions for the CO₂ impact assessment are detailed in the following table.

Current maximum CO anasification	2.0 mal9/								
Current maximum CO ₂ specification	2.9 mol%								
	4 mol%.								
Future maximum CO ₂ specification	Commingled CATS flow likely to be lower								
- '	No account taken of any blending of Teesside sourced gas								
	with other gas of low CO ₂ content in the NTS								
Assessment period	2019 to 2030								
Annual requirement for CO ₂	Scenario 1 – Non removal								
removal	Scenario 2 – Reduction to 2.9 mol% 365 days/yr								
Temoval	Scenario 3 – Reduction to 2.9 mol% 30 days/yr								
	Offshore - representative production from field operator								
Gas production profiles	Onshore – representative flows during summer maintenance								
	days								
Amine unit costs	Estimates from BP for fully installed systems								
Amine unit efficiency	97%								
Temperature required for stored	20°C (manufacturar data)								
amine when not in use	20°C (manufacturer data)								
Heating requirement for stored	0.71004								
amine	3.7MW								
	No account is taken of increased emissions from the								
Florida'' 110 contacts of	electrical power required to operate CO ₂ removal equipment								
Electricity, HC emissions	or from emissions from burning hydrocarbons emitted during								
	CO ₂ removal								
	DECC Updated Energy & Emissions Projections -								
ETS Carbon Valuation	September 2014, 'Carbon Prices - Industry and Services'								
	upto 2035 (2036+ Traded price equals non-traded price)								
	DECC Updated Energy & Emissions Projections -								
Carbon Valuation with Carbon Price	September 2014, 'Carbon Prices - Electricity Supply Sector'								
Support	up to 2035 (2036+ inflated at 6% per year)								
	DECC Appraisal Guide 2014, Table 1-20: supporting the								
Carbon Valuation 'Non Traded'	toolkit and guidance - Central Prices								
	DECC Updated Energy & Emissions Projections -								
Total UK Forecast CO ₂ Emissions	September 2014, Annex B Carbon Dioxide Emissions by								
_	Source								
	Gas Usage split by gas demand Users (ETS, Carbon								
Emissions cost by User Group	Support, non-ETS) – National Grid, Future-Energy-Scenarios								
	pg.168								
	All costs have been discounted using a 10% discount factor								
Net Present Value Discount Factor	back to a start date of 1/1/15								

Analysis

The detailed analysis is shown in the accompanying tables and spreadsheet. The summary of the output of the analysis is shown in the following table:

Assessment of CO ₂ Impact from Teesside Gas (2019-2030)	Scenario 1 NTS Delivery at 4 mol % CO2	Scenario 2 Offshore CO2 Reduction	Scenario 3 Onshore CO2 Reduction
CO ₂ Removed by Amine unit (4 mol% to 2.9 mol%) (te)	0	476,875	66,243
CO ₂ in fuel gas consumed by Amine unit (te)	0	219,920	172,046
CO ₂ above 2.9 mol% emitted by consumers (te)	64,256	0	0
Total additional CO ₂ emissions (te)	64,256	696,795	238,289

Cost Assessment of CO₂ from Teesside Gas (2019-2030) (£ NVP10 1/1/15)	Scenario 1 NTS Delivery at 4 mol % CO2	Scenario 2 Offshore CO2 Removal	Scenario 3 Onshore CO2 Removal
CO ₂ Total ETS Traded Cost	£42,232	£1,741,921	£578,525
CO ₂ Total Traded Cost with Carbon Price Support	£269,723		
Total CO2 Cost (Traded & Price Support)	£311,954	£1,741,921	£578,525
CO ₂ Total Non-Traded Cost (£/yr) (non-ETS consumption)	£959,753	£0	£0
Total Estimated Emissions Cost	£1,271,707	£1,741,921	£578,525
Estimated Fully Installed Cost of Amine Unit		£147,189,400	£129,089,543
Estimated Abatement Cost for additional CO2 prior to NTS entry		£148,931,320	£129,668,068
Cost per tonne	£20	£214	£544

Conclusions

- The least impact on CO₂ emissions from bringing gas with up to 4.0 mol% CO₂ content into the CATS system is for such gas to be allowed to flow into the NTS.
- Significantly more CO₂ is emitted by removing CO₂ from the gas. This is due to the fact that CO₂ removal using amine requires process heat. The highest level of emissions is attributed to reduction of CO₂ offshore as a result of operation of an amine unit on the total field gas export stream each day of operation. Onshore reduction of CO₂ has lower CO₂ emissions as the unit would only be used on days when CO₂ levels are expected to be elevated. However this is still significantly higher than an NTS delivery scenario as, when not in use, amine is required to be stored at 20°C to maintain its operational effectiveness and this requires further process heat.
- When considering cost of emissions from ETS participants, the impact of CO₂ removal is carried through with transport of 4.0 mol% CO₂ gas onto the NTS being the lowest cost option and reduction of CO₂ content offshore being the highest cost option
- If the cost of non-traded emissions is included then the cost to consumers of NTS gas from accepting gas with higher CO₂ content increases. However, if non-traded emissions are considered, BP and TGPP believe that the total cost of mitigating the CO₂ content of gas entering the NTS from Teesside should be taken into account.
- The cost of installing an amine unit either at specific fields offshore or at the onshore terminals is
 considerable. Current estimates for the fully installed cost of an offshore amine unit is of the order of
 £200m (undiscounted). When this is taken into account, the mitigation cost increases significantly when
 compared to costs to NTS gas consumers. On a tonnage basis the cost to an NTS gas consumer is c.
 £20/te but could cost up to £500/te to mitigate the CO₂ prior to gas entering the NTS.

CATS CO2 Impact Assessment (Amine Unit Capex Excluded)

	Total CO2 (Te)	NPV10	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	Total	Annual Avera
Reference Data																				
Number of Days Terminals anticipate CO2 in excess of 2.9 Mol %							30	30	30	30	30	30	30	30	30	30	30	30		l
Forecast CO2 content when in excess of 2.9 Mol%							4.0%	4.0%	4.0%	4.0%	4.0%	3.8%	3.6%	3.4%	3.4%	3.2%	3.2%	3.2%		ı
CO2 Emissions from warm Amine when unit not in use (Kg/hr)							718.51	718.51	718.51	718.51	718.51	718.51	718.51	718.51	718.51	718.51	718.51	718.51		1
Carbon Valuation 'Traded' (£/te C02)							5	5	6	6	6	6	6	7	7	7	7	8		1
Carbon Valuation 'Traded' with Carbon Price Support (£/te C02)							22	27	33	39	44	50	56	60	65	69	74	78		1
Carbon Valuation 'Non Traded' (£/te CO2)							66	67	68	69	70	71	72	73	74	75	77	78		1
Gas Price (p/th)							58.00	60.29	62.57	64.86	67.15	69.44	71.73	72.54	73.35	74.10	75.11	76.37		72
Total UK Forecast CO2 Emissions (MtCO2)							370	349	339	329	324	317	306	300	296	292	296	293	6,609	300
Scenario 1 - NTS Delivery at 4mol%																				ì
Additional CO2 emissions from 4mol% to 2.9mol% (te/CO2)	64.256						6,802	7,563	7,563	7,563	7,563	6,338	5,113	3,879	3,879	2,664	2,664	2,664	64,256	5,35
Cost of 'Traded' emissions (£)	- ,,	£42,232	-				9,120	10,517	10,908	11,313	11,734	10,199	8,535	6,716	6,965	4,962	5,146	5,337	101,451	8,4
Cost of 'Traded' emissions with Carbon Price Support (£)		£269,723					35,203	49,476	59,814	70,153	80,492	76,123	68,405	56,046	60,198	44,195	47,046	49,897	697,049	58,0
Total Cost of Traded & Traded with Price Support emissions (£)		£311,954					44,323	59,992	70,722	81,466	92,226	86,322	76,940	62,762	67,163	49,156	52,192	55,235	798,500	66,5
(-)							.,,		,		,	,	,	,	,	,	,		110,000	1
Cost of 'Non Traded' emissions (£)		£959,753	-	-		-	224,482	253,349	257,130	260,911	264,693	225,001	184,084	141,593	143,532	99,909	102,573	103,905	2,261,163	188,4
Total Cost of emissions (£)		£1,271,707	-				268,806	313,341	327,852	342,378	356,919	311,323	261,024	204,354	210,695	149,065	154,765	159,140	3,059,663	254,97
Scenario 2 - Offshore removal																		ĺ		ı
Field Forecast Flow (mscfd)							153	259	264	264	264	229	178	147	125	106	93	82		
Field Forecast Flow (mscf/year)							55,725	94,695	96,455	96,455	96,455	83,511	65,000	53,505	45,586	38,871	33,824	30,053	790,135	65,8
CO2 emissions from amine process to 2.9mol% content (te)	476,875						33,530	57,001	58,119	58,119	58,119	50,668	39,119	32,413	27,569	23,471	20,491	18,255	476,875	39,7
Additional CO2 emissions from Amine unit fuel gas (te)	219,920						15,463	26,287	26,803	26,803	26,803	23,367	18,040	14,948	12,714	10,824	9,450	8,419	219,920	18,32
Total CO2 emissions from Offshore removal (te)	696,795						48,993	83,289	84,922	84,922	84,922	74,034	57,159	47,360	40,283	34,295	29,940	26,674	696,795	58,0
Total cost of emissions (£)		£1,741,921	-				252,645	445,466	471,089	488,605	506,772	458,228	366,934	315,335	278,189	245,643	222,424	205,527	4,256,856	354,73
	<u> </u>																			\vdash
Scenario 3 - Onshore removal																				.
Terminals Forecast Flow When Exceeding 2.9 mol% (mscfd)							360	400	400	400	400	400	400	400	400	400	400	400	4,760	3:
CO2 emissions from amine process (4 mol% to 2.9mol% content (te)	66,243						7,013	7,797	7,797	7,797	7,797	6,534	5,272	3,999	3,999	2,747	2,747	2,747	66,243	5,5
Additional CO2 emissions from Amine unit fuel gas (te)	32,304						3,207	3,565	3,565	3,565	3,565	3,145	2,678	2,152	2,152	1,570	1,570	1,570	32,304	2,6
Additional CO2 emissions from Amine when not in use (te)	139,741						11,645	11,645	11,645	11,645	11,645	11,645	11,645	11,645	11,645	11,645	11,645	11,645	139,741	11,6
Total C02 emissions from Onshore removal (te)	238,289						21,865	23,007	23,007	23,007	23,007	21,324	19,595	17,797	17,797	15,961	15,961	15,961	238,289	19,8
Total cost of emissions (£)		£578.525	-				112,751	123.051	127.626	132.372	137.294	131.984	125,790	118.493	122.899	114,324	118,575	122.984	1.488.144	124,0

CATS CO2 Full Cycle Cost/Benefit Analysis

	Total CO2 (Te)	NPV10	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	Total	Annual Avera
deference Data																		l		
ield Forecast export Flow (th/year)							1,329,422,233	1,476,241,519	1,476,241,519	1,476,241,519	1,476,241,519	1,476,241,519	1,476,241,519	1,476,241,519	1,476,241,519	1,476,241,519	1,476,241,519	1,476,241,519	17,568,078,938	1,464,006
umber of Days Terminals anticipate CO2 in excess of 2.9 Mol %							30	30	30	30	30	30	30	30	30	30	30	30		
precast CO2 content when in excess of 2.9 Mol%							4.0%	4.0%	4.0%	4.0%	4.0%	3.8%	3.6%	3.4%	3.4%	3.2%	3.2%	3.2%		
arbon Valuation 'Traded' (£/te CO2)							5	5	6	6	6	6	6	7	7	7	7	8		
Carbon Valuation 'Traded' with Carbon Price Support (£/te CO2)							22	27	33	39	44	50	56	60	65	69	74	78		
arbon Valuation 'Non Traded' (£/te CO2)							66	67	68	69	70	71	72	73	74	75	77	78		
Gas Price (p/th)							58.00	60.29	62.57	64.86	67.15	69.44	71.73	72.54	73.35	74.10	75.11	76.37		
Total UK Forecast C02 Emissions (MtC02)							370	349	339	329	324	317	306	300	296	292	296	293	6,609	
Scenario 1 - NTS Delivery at 4mol%																				
Additional CO2 emissions from 4mol% to 2.9mol% (te/CO2)	64,256						6,802	7,563	7,563	7,563	7,563	6,338	5,113	3,879	3,879	2,664	2,664	2,664	64,256	
Cost of 'Traded' emissions (£)		£42,232	-	-	-	-	9,120	10,517	10,908	11,313	11,734	10,199	8,535	6,716	6,965	4,962	5,146	5,337	101,451	6
Cost of 'Traded' emissions with Carbon Price Support (£)		£269,723	-	-	-	-	35,203	49,476	59,814	70,153	80,492	76,123	68,405	56,046	60,198	44,195	47,046	49,897	697,049	4
Total Cost of Traded & Traded with Price Support (£)		£311,954	-	-	-	-	44,323	59,992	70,722	81,466	92,226	86,322	76,940	62,762	67,163	49,156	52,192	55,235	798,500	4
Cost of 'Non Traded' emissions (£)		£959,753	-	-	-	-	224,482	253,349	257,130	260,911	264,693	225,001	184,084	141,593	143,532	99,909	102,573	103,905	2,261,163	141
Total Cost of emissions (£)		£1.271.707				-	268.806	313.341	327.852	342,378	356,919	311.323	261.024	204.354	210.695	149.065	154,765	159.140	3.059.663	19:
Scenario 2 - Offshore removal Field Forecast Flow (mscfd)							153	259	264	264	264	229	178	147	125	106	93	82		
Field Forecast Flow (mscf/year)							55,725	94,695	96,455	96,455	96,455	83,511	65,000	53,505	45,586	38,871	33,824	30,053	790,135	6
202 emissions from amine process to 2.9mol% content (te)	476,875						33,530	57,001	58,119	58,119	58,119	50,668	39,119	32,413	27,569	23,471	20,491	18,255	476,875	3
Additional CO2 emissions from Amine unit fuel gas (te)	219,920						15,463	26,287	26,803	26,803	26,803	23,367	18,040	14,948	12,714	10,824	9,450	8,419	219,920	1
Total CO2 emissions from Offshore removal (te)	696,795						48,993	83,289	84,922	84,922	84,922	74,034	57,159	47,360	40,283	34,295	29,940	26,674	696,795	5
Capex of Amine unit (£)		£129,089,543	-	-	90,000,000	90,000,000		-		-		-	-	-		-		-	180,000,000	11,25
Total Cost of Emissions		£1,741,921	-	-	-		252,645	445,466	471,089	488,605	506,772	458,228	366,934	315,335	278,189	245,643	222,424	205,527	4,256,856	26
Total cost of emissions (£)		£130,831,464		-	90,000,000	90,000,000	252,645	445,466	471.089	488,605	506,772	458,228	366,934	315,335	278,189	245.643				
TOTAL COST OF GUIDSTONS (E)																243,043	222,424	205,527	184,256,856	
Total cost of emissions (E)									,	•						243,043	222,424	205,527	184,256,856	11,516
																243,043	222,424	205,527	184,256,856	
Scenario 3 - Onshore removal							360	400	400	400	400	400	400	400	400	400	222,424 400	205,527	184,256,856 4,760	
icenario 3 - Onshore removal erminals Forecast Flow When Exceeding 2.9 mol% (mscfd)	66,243						360 7,013	400 7,797	400 7,797	400 7,797	400 7,797	400 6,534	400 5,272	400 3,999	400 3,999					11,51
Scenario 3 - Onshore removal Terminals Forecast Flow When Exceeding 2.9 mol% (mscfd) CU2 emissions from amine process (4 mol% to 25 mol% content (te) Additional CU2 emissions from Amine unit fuel gas (the)	66,243 32,304															400	400	400	4,760	11,51
iscenario 3 - Onshore removal ferminals Forecast Flow When Exceeding 2.9 mol% (mscfd) 202 emissions from amine process (4 mol % to 2.9 mol % content (te) additional CIQ emissions from Amine unit fuel gas (te)							7,013	7,797	7,797	7,797	7,797	6,534	5,272	3,999	3,999	400 2,747	400 2,747	400 2,747	4,760 66,243	11,51
icenario 3 - Onshore removal erminals Forecast Flow When Exceeding 2.9 mol% (mscfd) grampinals Forecast Flow When Exceeding 2.9 mol% content (te) ddditional CO2 emissions from Amine unit Tuel gas (te) ddditional CO2 emissions from Amine when not in use (te)	32,304						7,013 3,207	7,797 3,565	7,797 3,565	7,797 3,565	7,797 3,565	6,534 3,145	5,272 2,678	3,999 2,152	3,999 2,152	400 2,747 1,570	400 2,747 1,570	400 2,747 1,570	4,760 66,243 32,304	11,51
Scenario 3 - Onshore removal Terminals Forecast Flow withen Exceeding 2.9 mol% (mscfd) QD2 emissions From amine process (4 mol% to 2.9 mol% content (te) Additional CO2 emissions from Amine unit fuel gas (te) Additional CO2 emissions from Amine when not in use (te) Total CO2 emissions from Onshore removal (te)	32,304 139,741	£147,189,400	_	50,000,000	50,000,000	100,000,000	7,013 3,207 11,645	7,797 3,565 11,645	7,797 3,565 11,645	7,797 3,565 11,645	7,797 3,565 11,645	6,534 3,145 11,645	5,272 2,678 11,645	3,999 2,152 11,645	3,999 2,152 11,645	400 2,747 1,570 11,645	400 2,747 1,570 11,645	400 2,747 1,570 11,645	4,760 66,243 32,304 139,741	11,51
Scenario 3 - Onshore removal Ferminals Forecast Flow When Exceeding 2.9 mol% (mscfd) OZ emissions From amine process (4 mol% to 2.9mol% content (te)	32,304 139,741		1	50,000,000	50,000,000	100,000,000	7,013 3,207 11,645 21,865	7,797 3,565 11,645 23,007	7,797 3,565 11,645 23,007	7,797 3,565 11,645 23,007	7,797 3,565 11,645 23,007	6,534 3,145 11,645 21,324	5,272 2,678 11,645 19,595	3,999 2,152 11,645 17,797	3,999 2,152 11,645 17,797	400 2,747 1,570 11,645 15,961	400 2,747 1,570 11,645 15,961	400 2,747 1,570 11,645	4,760 66,243 32,304 139,741 238,289	

Scenario 1 - NTS Delivery at up to 4 mol% for Train 2

Case	Check	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030
Full Field [MMSCFD]	450	180	200	200	200	200	200	200	200	200	200	200	200
Full Field [kSm³/hr]	530.5	212.4	236.0	236.0	236.0	236.0	236.0	236.0	236.0	236.0	236.0	236.0	236.0
Outlet Flow Pre-Treatement [MMSCFD]	429	172	191	191	191	191	191	191	191	191	191	191	191
Outlet Flow Pre-Treatement [kSm³/hr]	506.5	202.7	225.1	225.1	225.1	225.1	225.1	225.1	225.1	225.1	225.1	225.1	225.1
Oulet Mass Flow Pre-Treatement [kg/hr]	398,369	159,289	176,716	176,716	176,716	176,716	176,716	176,716	176,716	176,716	176,716	176,716	176,716
Outlet Molecular Weight Pre-Treatement [kmol/kg]	18.63	18.62	18.60	18.60	18.60	18.60	18.60	18.60	18.60	18.60	18.60	18.60	18.60
CO2 Content Pre-Treatement [mol%]	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01
CO2 Content Pre-Treatement [mol%]	3.40%	3.56%	3.56%	3.56%	3.56%	3.56%	3.56%	3.56%	3.56%	3.56%	3.56%	3.56%	3.56%
Quantities of CO2 Delivered [kg/hr]	31,993	13,400	14,880	14,880	14,884	14,880	14,880	14,880	14,880	14,880	14,880	14,880	14,880
Quantities of CO2 Delivered [te per annum]	280,258	117,384	130,348	130,348	130,384	130,348	130,348	130,348	130,348	130,348	130,348	130,348	130,348
CO2 Removal Unit Flow [MMSCFD]	67	34	37	37	37	37	37	37	37	37	37	37	37
CO2 Removal Unit Flow [kSm³/hr]	79.6	39.8	44.2	44.2	44.2	44.2	44.2	44.2	44.2	44.2	44.2	44.2	44.2
Quantities of CO2 removed [kg/hr]	4,878	2,551	2,832	2,832	2,836	2,832	2,832	2,832	2,832	2,832	2,832	2,832	2,832
Export Flow Post-Treatement [MMSCFD]	428.1	170.7	189.5	189.5	189.5	189.5	189.5	189.5	189.5	189.5	189.5	189.5	189.5
Export Flow Post-Treatement [kSm³/hr]	505.1	201.3	223.6	223.6	223.6	223.6	223.6	223.6	223.6	223.6	223.6	223.6	223.6
Export Mass Flow Post-Treatement [kg/hr]	393,491	156,738	173,883	173,883	173,879	173,883	173,883	173,883	173,883	173,883	173,883	173,883	173,883
Export Molecular Weight Post-Treatement [kmol/kg]	18.45	18.44	18.42	18.42	18.42	18.42	18.42	18.42	18.42	18.42	18.42	18.42	18.42
CO2 Molecular Weight Post-Treatement [kmol/kg]	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01
CO2 Content Post-Treatement [mol%]	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%
Quantities of CO2 Delivered [kg/hr]	27,040	10,778	11,969	11,969	11,969	11,969	11,969	11,969	11,969	11,969	11,969	11,969	11,969
Quantities of CO2 Delivered [te per annum]	236,874	94,418	104,849	104,849	104,847	104,849	104,849	104,849	104,849	104,849	104,849	104,849	104,849
Additional CO2 emissions [kg/hr]	4,953	2,622	2,911	2,911	2,915	2,911	2,911	2,911	2,911	2,911	2,911	2,911	2,911
Additional CO2 emissions Scenario 1 [te per annum]	43,385	1,888	2,096	2,096	2,099	2,096	2,096	2,096	2,096	2,096	2,096	2,096	2,096

Scenario 1 - NTS Delivery at up to 4 mol% for CATS

Case	Check	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030
Full Field [MMSCFD]	900	180	200	200	200	200	200	200	200	200	200	200	200
Full Field [kSm³/hr]	1061.9	212.4	236.0	236.0	236.0	236.0	236.0	236.0	236.0	236.0	236.0	236.0	236.0
Outlet Flow Pre-Treatement [MMSCFD]	874	172	191	191	191	191	191	191	191	191	191	191	191
Outlet Flow Pre-Treatement [kSm³/hr]	1030.8	202.7	225.1	225.1	225.1	225.1	225.1	225.1	225.1	225.1	225.1	225.1	225.1
Oulet Mass Flow Pre-Treatement [kg/hr]	833,193	159,289	176,716	176,716	176,716	176,716	176,716	176,716	176,716	176,716	176,716	176,716	176,716
Outlet Molecular Weight Pre-Treatement [kmol/kg]	19.15	18.62	18.60	18.60	18.60	18.60	18.60	18.60	18.60	18.60	18.60	18.60	18.60
CO2 Content Pre-Treatement [mol%]	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01
CO2 Content Pre-Treatement [mol%]	3.51%	3.51%	3.51%	3.51%	3.51%	3.51%	3.51%	3.51%	3.51%	3.51%	3.51%	3.51%	3.51%
Quantities of CO2 Delivered [kg/hr]	67,210	13,225	14,685	14,685	14,685	14,685	14,685	14,685	14,685	14,685	14,685	14,685	14,685
Quantities of CO2 Delivered [te per annum]	588,762	115,849	128,643	128,643	128,643	128,643	128,643	128,643	128,643	128,643	128,643	128,643	128,643
CO2 Removal Unit Flow [MMSCFD]	162	32	35	35	35	35	35	35	35	35	35	35	35
CO2 Removal Unit Flow [kSm³/hr]	190.6	37.6	41.7	41.7	41.7	41.7	41.7	41.7	41.7	41.7	41.7	41.7	41.7
Quantities of CO2 removed [kg/hr]	12,053	2,379	2,642	2,642	2,642	2,642	2,642	2,642	2,642	2,642	2,642	2,642	2,642
Export Flow Post-Treatement [MMSCFD]	868.1	170.8	189.7	189.7	189.7	189.7	189.7	189.7	189.7	189.7	189.7	189.7	189.7
Export Flow Post-Treatement [kSm³/hr]	1024.2	201.6	223.8	223.8	223.8	223.8	223.8	223.8	223.8	223.8	223.8	223.8	223.8
Export Mass Flow Post-Treatement [kg/hr]	821,140	156,909	174,074	174,074	174,074	174,074	174,074	174,074	174,074	174,074	174,074	174,074	174,074
Export Molecular Weight Post-Treatement [kmol/kg]	18.99	18.44	18.42	18.42	18.42	18.42	18.42	18.42	18.42	18.42	18.42	18.42	18.42
CO2 Molecular Weight Post-Treatement [kmol/kg]	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01
CO2 Content Post-Treatement [mol%]	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%
Quantities of CO2 Delivered [kg/hr]	54,806	10,786	11,978	11,978	11,978	11,978	11,978	11,978	11,978	11,978	11,978	11,978	11,978
Quantities of CO2 Delivered [te per annum]	480,101	94,486	104,926	104,926	104,926	104,926	104,926	104,926	104,926	104,926	104,926	104,926	104,926
													1
Additional CO2 emissions [kg/hr]	12,404	2,439	2,707	2,707	2,707	2,707	2,707	2,707	2,707	2,707	2,707	2,707	2,707
Additional CO2 emissions Scenario 1 [te per annum]	108,660	1,756	1,949	1,949	1,949	1,949	1,949	1,949	1,949	1,949	1,949	1.949	1,949
Additional CO2 emissions Scenario 1 [te per annum]	108,660	1,750	1,949	1,949	1,949	1,949	1,949	1,949	1,949	1,949	1,949	1,949	1,949

Scenario 2 - Onshore CO2 Removal for Train 2

Case	Check	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030
Full Field [MMSCFD]	450	180	200	200	200	200	200	200	200	200	200	200	200
Full Field [kSm³/hr]	530.5	212.4	236.0	236.0	236.0	236.0	236.0	236.0	236.0	236.0	236.0	236.0	236.0
Inlet Molecular Weight	20.3	20.3	20.3	20.3	20.3	20.3	20.3	20.3	20.3	20.3	20.3	20.3	20.3
Inlet Molecular Weight	20.5	20.3	20.3	20.5	20.3	20.3	20.3	20.3	20.3	20.5	20.5	20.5	20.3
CO2 Content In [mol%]	4.00%	4.00%	4.00%	4.00%	4.00%	4.00%	3.80%	3.60%	3.40%	3.40%	3.20%	3.20%	3.20%
CO2 Content Out [mol%]	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%
cor content out (mone)	2.00%	2.0070	2.0070	2.0070	2.0070	2.00/0	2.0070	2.0070	2.0070	2.0070	2.0070	2.0070	2.0070
Outlet Flow Pre-Treatement [MMSCFD]	429.3	171.8	190.8	190.8	190.8	190.8	190.8	190.8	190.8	190.8	190.8	190.8	190.8
Outlet Flow Pre-Treatement [kSm³/hr]	506.5	202.7	225.1	225.1	225.1	225.1	225.1	225.1	225.1	225.1	225.1	225.1	225.1
Oulet Mass Flow Pre-Treatement [kg/hr]	398,369	159,289	176,716	176,716	176,716	176,716	176,716	176,716	176,716	176,716	176,716	176,716	176,716
Outlet Molecular Weight Pre-Treatement	18.63	18.62	18.60	18.60	18.60	18.60	18.60	18.60	18.60	18.60	18.60	18.60	18.60
CO2 Content Pre-Treatement [mol%]	4.19%	4.19%	4.19%	4.19%	4.19%	4.19%	3.98%	3.77%	3.56%	3.56%	3.36%	3.36%	3.36%
Shrink Factor	0.9549	0.9543	0.9538	0.9538	0.9538	0.9538	0.9538	0.9538	0.9538	0.9538	0.9538	0.9538	0.9538
January Color	0.5515	0.5515	0.5550	0.5550	0.5550	0.5550	0.5550	0.5550	0.5550	0.5550	0.5550	0.5550	0.5550
CO2 Removal Unit Flow [MMSCFD]	138	55	62	62	62	62	54	47	38	38	28	28	28
CO2 Removal Unit Flow [kSm³/hr]	163.1	65.3	72.7	72.7	72.7	72.7	64.3	54.9	44.4	44.4	32.8	32.8	32.8
continuous cinerion (tom /m)	105.1	03.3	72.7	72.7	72.7	72.7	01.5	54.5			52.0	52.0	32.0
CO2 Content Exit Unit [ppm]	1257	1257	1258	1258	1258	1258	1195	1132	1069	1069	1007	1007	1007
Removal Unit Efficiency [%]	97%	97%	97%	97%	97%	97%	97%	97%	97%	97%	97%	97%	97%
7.5		. ,-											
Quantities of CO2 removed [kg/hr]	12,311	4,935	5,491	5,491	5,491	5,491	4,614	3,737	2,854	2,854	1,984	1,984	1,984
Quantities of CO2 removed [te per annum (30 days/yr)]	107,847	3,553	3,953	3,953	3,953	3,953	3,322	2,691	2,055	2,055	1,428	1,428	1,428
CO2 Molecular Weight [kmol/kg]	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01
Quantities of Hydrocarbons (assumed 1 mol%) [kg/hr]	44.88	17.99	20.02	20.02	20.02	20.02	16.82	13.62	10.40	10.40	7.23	7.23	7.23
Methane Molecular Weight [kmol/kg]	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04
Quantities of VOC removed (assumed as 500 ppm) [kg/hr]	10.93	4.38	4.87	4.87	4.87	4.87	4.09	3.32	2.53	2.53	1.76	1.76	1.76
Benzene Molecular Weight [kmol/kg]	78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11
Export Flow Post-Treatement [MMSCFD]	420.0	168.1	186.6	186.6	186.6	186.6	187.6	188.5	189.5	189.5	190.4	190.4	190.4
Export Flow Post-Treatement [kSm³/hr]	495.6	198.3	220.2	220.2	220.2	220.2	221.3	222.4	223.6	223.6	224.7	224.7	224.7
Export Mass Flow Post-Treatement [kg/hr]	386,058	154,354	171,225	171,225	171,225	171,225	172,102	172,978	173,862	173,862	174,732	174,732	174,732
Export Molecular Weight Post-Treatement	18.45	18.44	18.42	18.42	18.42	18.42	18.42	18.42	18.42	18.42	18.42	18.42	18.42
CO2 Content Post-Treatement [mol%]	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%
	MEA												
Gas Flowrate [MMSCFD]	138	55	62	62	62	62	54	47	38	38	28	28	28
Sour Gas Processed, Q [MSm³/day]	3.91	1.57	1.74	1.74	1.74	1.74	1.54	1.32	1.07	1.07	0.79	0.79	0.79
Contactor Pressure, P [kPa abs]	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33
Acid Gas Conc ⁿ , y [mole%]	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033
Amine Concn, x [mass%]	20	20	20	20	20	20	20	20	20	20	20	20	20
mol acid gas pick-up per mol amine	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33
Amine Flow, [m³/hr]	274.78	110.08	122.40	122.40	122.40	122.40	108.27	92.57	74.88	74.88	55.28	55.28	55.28
Amine Flow, [m ³ /d]	6594.74	2642.03	2937.72	2937.72	2937.72	2937.72	2598.57	2221.74	1797.08	1797.08	1326.76	1326.76	1326.76
Amine Flow, [GPM]	1209.82	484.69	538.93	538.93	538.93	538.93	476.71	407.58	329.68	329.68	243.40	243.40	243.40
Amine Contactor Diameter, Dc [mm]	2028	1284	1353	1353	1353	1353	1273	1177	1059	1059	910	910	910
Absorbed Reboiler Duty [MW]	25.55	10.24	11.38	11.38	11.38	11.38	10.07	8.61	6.96	6.96	5.14	5.14	5.14
Heater Duty [MW]	28.39	11.38	12.65	12.65	12.65	12.65	11.19	9.57	7.74	7.74	5.71	5.71	5.71
Thermal Efficiency at 90%	90%	90%	90%	90%	90%	90%	90%	90%	90%	90%	90%	90%	90%
Fuel Gas HHV [MJ/kg]	46.990	47.131	47.080	47.080	47.080	47.080	47.080	47.080	47.080	47.080	47.080	47.080	47.080
Fuel Gas Requirement [kg/hr]	2175	869	967	967	967	967	856	731	592	592	437	437	437
CO2 Emissions Factor [kg CO2 per kg FG]	2.577	2.575	2.573	2.573	2.573	2.573	2.573	2.573	2.573	2.573	2.573	2.573	2.573
CO2 Formed from Operational Amine Unit FG [kg/hr]	5605	2237	2489	2489	2489	2489	2201	1882	1522	1522	1124	1124	1124
CO2 Formed from Operational Amine Unit FG [te per annum (30 days)]	49,101	1,611	1,792	1,792	1,792	1,792	1,585	1,355	1,096	1,096	809	809	809
			1	ļ	ļ							ļ	ļ
Heater Duty for amine heating when non-operational [MW]	3.664	3.664	3.664	3.664	3.664	3.664	3.664	3.664	3.664	3.664	3.664	3.664	3.664
FG Requirement for non-operational Amine Unit (kg/hr)	281	280.706	280.706	280.706	280.706	280.706	280.706	280.706	280.706	280.706	280.706	280.706	280.706
CO2 Formed in Standby Mode [kg/hr]	723	723.293	723.293	723.293	723.293	723.293	723.293	723.293	723.293	723.293	723.293	723.293	723.293
	5.815	5.815	5.815	5,815	5,815	5,815	5,815	5,815	5,815	5,815	5,815	5,815	5,815
CO2 Formed in Standby Mode [te per annum (335 days)]	3,013	3,013	3,013	3,013	-,	,	.,	.,					•

Scenario 2 - Onshore CO2 Removal for CATS

Case	Check		2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030
Full Field [MMSCFD]	500		180	200	200	200	200	200	200	200	200	200	200	200
Full Field [kSm³/hr]	589.5		212.4	236.0	236.0	236.0	236.0	236.0	236.0	236.0	236.0	236.0	236.0	236.0
Inlet Molecular Weight	20.3		20.3	20.3	20.3	20.3	20.3	20.3	20.3	20.3	20.3	20.3	20.3	20.3
micrimorecala Weight	20.5		20.5	20.5	20.5	20.5	20.5	20.5	20.5	20.5	20.5	20.5	20.5	20.3
CO2 Content In [mol%]	3.40%		4.00%	4.00%	4.00%	4.00%	4.00%	3.80%	3.60%	3.40%	3.40%	3.20%	3.20%	3.20%
CO2 Content Out [mol%]	2.88%		2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%
Outlet Flow Pre-Treatement [MMSCFD]	483.4		173.8	193.2	193.2	193.2	193.2	193.2	193.2	193.2	193.2	193.2	193.2	193.2
Outlet Flow Pre-Treatement [kSm³/hr]	570.3		205.1	227.9	227.9	227.9	227.9	227.9	227.9	227.9	227.9	227.9	227.9	227.9
Oulet Mass Flow Pre-Treatement [kg/hr]	460,486		165,388	183,798	183,798	183,798	183,798	183,798	183,798	183,798	183,798	183,798	183,798	183,798
Outlet Molecular Weight Pre-Treatement	19.13		19.10	19.10	19.10	19.10	19.10	19.10	19.10	19.10	19.10	19.10	19.10	19.10
CO2 Content Pre-Treatement [mol%]	3.51%		4.14%	4.14%	4.14%	4.14%	4.14%	3.93%	3.73%	3.52%	3.52%	3.31%	3.31%	3.31%
Shrink Factor	0.9675		0.9658	0.9659	0.9659	0.9659	0.9659	0.9659	0.9659	0.9659	0.9659	0.9659	0.9659	0.9659
CO2 Removal Unit Flow [MMSCFD]	90		55	61	61	61	61	53	45	36	36	26	26	26
CO2 Removal Unit Flow [kSm³/hr]	105.8		64.4	71.5	71.5	71.5	71.5	62.9	53.4	42.6	42.6	30.7	30.7	30.7
CO2 Content Exit Unit [ppm]	1054		1242	1242	1242	1242	1242	1180	1118	1056	1056	994	994	994
Removal Unit Efficiency [%]	97%		97%	97%	97%	97%	97%	97%	97%	97%	97%	97%	97%	97%
Quantities of CO2 removed [kg/hr]	6,695		4,805	5,338	5,338	5,338	5,338	4,461	3,584	2,701	2,701	1,831	1,831	1,831
Quantities of CO2 removed [te per annum (30 days/yr)]	58,649	720	3,460	3,843	3,843	3,843	3,843	3,212	2,581	1,945	1,945	1,318	1,318	1,318
CO2 Molecular Weight [kmol/kg]	44.01		44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01
Quantities of Hydrocarbons (assumed 1 mol%) [kg/hr]	24.41		17.52	19.46	19.46	19.46	19.46	16.26	13.07	9.85	9.85	6.67	6.67	6.67
Methane Molecular Weight [kmol/kg]	16.04		16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04
Quantities of VOC removed (assumed as 500 ppm) [kg/hr]	5.94		4.26	4.74	4.74	4.74	4.74	3.96	3.18	2.40	2.40	1.62	1.62	1.62
Benzene Molecular Weight [kmol/kg]	78.11		78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11
Export Flow Post-Treatement [MMSCFD]	480.2		170.1	189.1	189.1	189.1	189.1	190.0	190.9	191.9	191.9	192.8	192.8	192.8
Export Flow Post-Treatement [kSm³/hr]	566.6		200.8	223.1	223.1	223.1	223.1	224.2	225.3	226.4	226.4	227.5	227.5	227.5
Export Mass Flow Post-Treatement [kg/hr]	453,790		160,583	178,460	178,460	178,460	178,460	179,337	180,214	181,097	181,097	181,967	181,967	181,967
Export Molecular Weight Post-Treatement	18.98		18.95	18.95	18.95	18.95	18.95	18.95	18.95	18.95	18.95	18.95	18.95	18.95
CO2 Content Post-Treatement [mol%]	2.88%		2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%	2.88%
o si i (autospi)	MEA		MEA	MEA	MEA	MEA								
Gas Flowrate [MMSCFD]	90		55	61	61	61	61	53	45	36	36	26	26	26
Sour Gas Processed, Q [MSm³/day]	2.54		1.55	1.72	1.72	1.72	1.72	1.51	1.28	1.02	1.02	0.74	0.74	0.74
Contactor Pressure, P [kPa abs]	12101.33		12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33
Acid Gas Conc ⁿ , y [mole%]	4.28033		4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033
Amine Concn, x [mass%]	20		20	20	20	20	20	20	20	20	20	20	20	20
mol acid gas pick-up per mol amine	0.33		0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33
Amine Flow, [m³/hr]	178.21		108.47	120.51	120.51	120.51	120.51	106.02	89.92	71.77	71.77	51.67	51.67	51.67
Amine Flow, [m³/d]	4277.12		2603.38	2892.31	2892.31	2892.31	2892.31	2544.48	2158.01	1722.49	1722.49	1240.14	1240.14	1240.14
Amine Flow, [GPM]	784.65		477.60	530.60	530.60	530.60	530.60	466.79	395.89	316.00	316.00	227.51	227.51	227.51
Amine Contactor Diameter, Dc [mm]	1633		1274	1343	1343	1343	1343	1260	1160	1036	1036	879	879	879
Absorbed Reboiler Duty [MW]	16.57		10.09	11.21	11.21	11.21	11.21	9.86	8.36	6.67	6.67	4.81	4.81	4.81
Heater Duty [MW]	18.42		11.21	12.45	12.45	12.45	12.45	10.96	9.29	7.42	7.42	5.34	5.34	5.34
Thermal Efficiency at 90%	90%		90%	90%	90%	90%	90%	90%	90%	90%	90%	90%	90%	90%
5 10 100/100/11	47.500		47 707	47 707	47.707	47 707	47.707	47 707	47 707	47 707	47 707	47 707	47 707	47 70-
Fuel Gas HHV [MJ/kg]	47.698		47.727	47.727	47.727	47.727	47.727	47.727	47.727	47.727	47.727	47.727	47.727	47.727
Fuel Gas Requirement [kg/hr]	1390		845	939	939	939	939	826	701	559	559	403	403	403
CO2 Fii Ft[lCO2 l FC]	2.622		2.622	2.622	2.622	2.622	2.622	2.622	2.622	2.622	2.622	2.622	2.622	2.622
CO2 Emissions Factor [kg CO2 per kg FG]	2.622		2.622	2.622	2.622	2.622	2.622	2.622	2.622	2.622	2.622	2.622	2.622	2.622
CO2 Formed from Amine Unit FG [kg/hr] CO2 Formed from Amine Unit FG [te per annum (30 days)]	3644 31,925		2217 1,596	2463 1,773	2463 1,773	2463 1,773	2463 1,773	2167 1,560	1838 1,323	1467 1,056	1467 1,056	1056 760	1056 760	1056 760
coz romea nom Amine omit ro [te per amium (30 days)]	31,923	L	1,390	1,//3	1,775	1,775	1,//5	1,300	1,323	1,030	1,030	700	700	700
Heater Duty for amine heating when non-operational [MW]	3.664		3.664	3.664	3.664	3.664	3.664	3.664	3.664	3.664	3.664	3.664	3.664	3.664
FG Requirement for non-operational Amine Unit (kg/hr)	277		276,539	276,539	276.539	276.539	276.539	276.539	276.539	276.539	276.539	276.539	276,539	276,539
CO2 Formed in Standby Mode [kg/hr]	725		725.104	725.104	725.104	725.104	725.104	725.104	725.104	725.104	725.104	725.104	725.104	725.104
				5,830			5,830						5,830	5,830
CO2 Formed in Standby Mode [te per annum (335 days)]														
CO2 Formed in Standby Mode [te per annum (335 days)]	5,830		5,830	5,830	5,830	5,830	5,830	5,830	5,830	5,830	5,830	5,830	3,630	3,630

Scenario 3 - Offshore CO2 Removal

Case	Design	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030
Full Field [MMSCFD]	300	153	259	264	264	264	229	178	147	125	106	93	82
Full Field [kSm³/hr]	353.7	180.0	305.9	311.5	311.5	311.5	269.7	209.9	172.8	147.2	125.6	109.3	97.1
CO2 Content In [mol%]	4.00%	4.00%	4.00%	4.00%	4.00%	4.00%	4.00%	4.00%	4.00%	4.00%	4.00%	4.00%	4.00%
CO2 Content Out [mol%]	2.74%	2.89%	2.89%	2.89%	2.89%	2.89%	2.88%	2.89%	2.88%	2.88%	2.89%	2.88%	2.88%
CO2 Removal Unit Flow [MMSCFD]	100	45	76.5	78	78	78	68	52.5	43.5	37	31.5	27.5	24.5
CO2 Removal Unit Flow [kSm³/hr]	117.9	53.1	90.2	92.0	92.0	92.0	80.2	61.9	51.3	43.6	37.1	32.4	28.9
,,						02.0					01112		
CO2 Content Exit Unit [ppm]	1249	1249	1249	1249	1249	1249	1249	1249	1249	1249	1249	1249	1249
Removal Unit Efficiency [%]	97%	97%	97%	97%	97%	97%	97%	97%	97%	97%	97%	97%	97%
Quantities of CO2 removed [kg/hr]	8,506	3,828	6,507	6,635	6,635	6,635	5,784	4,466	3,700	3,147	2,679	2,339	2,084
Quantities of CO2 removed [te per annum]	74,512	33,530	57,001	58,119	58,119	58,119	50,668	39,119	32,413	27,569	23,471	20,491	18,255
CO2 Molecular Weight [kmol/kg]	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01	44.01
Quantities of Hydrocarbons (assumed 1 mol%) [kg/hr]	31.01	13.95	23.72	24.19	24.19	24.19	21.08	16.28	13.49	11.47	9.77	8.53	7.60
Methane Molecular Weight [kmol/kg]	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04	16.04
Quantities of VOC removed (assumed as 500 ppm) [kg/hr]	7.55	3.40	5.77	5.89	5.89	5.89	5.13	3.96	3.28	2.79	2.38	2.08	1.85
Benzene Molecular Weight [kmol/kg]	78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11	78.11
	MEA												
Gas Flowrate [MMSCFD]	100	45	76.5	78	78	78	68	52.5	43.5	37	31.5	27.5	24.5
Sour Gas Processed, Q [MSm ³ /day]	2.83	1.27	2.17	2.21	2.21	2.21	1.93	1.49	1.23	1.05	0.89	0.78	0.69
Contactor Pressure, P [kPa abs]	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33	12101.33
Acid Gas Conc ⁿ , y [mole%]	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033	4.28033
Amine Concn, x [mass%]	20	20	20	20	20	20	20	20	20	20	20	20	20
mol acid gas pick-up per mol amine	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33	0.33
Amine Flow, [m ³ /hr]	198.78	89.45	152.06	155.05	155.05	155.05	135.17	104.36	86.47	73.55	62.61	54.66	48.70
Amine Flow, [m³/d]	4770.65	2146.79	3649.54	3721.10	3721.10	3721.10	3244.04	2504.59	2075.23	1765.14	1502.75	1311.93	1168.81
Amine Flow, [GPM]	875.19	393.83	669.52	682.65	682.65	682.65	595.13	459.47	380.71	323.82	275.68	240.68	214.42
Annie How, [Grwi]	873.13	393.83	009.32	062.03	062.03	062.03	333.13	433.47	360.71	323.62	273.00	240.00	214.42
Amine Contactor Diameter, Dc [mm]	1725	1157	1509	1523	1523	1523	1422	1250	1138	1049	968	904	854
runne contactor planteter, po [mm]	17.20	1107	1505	1020	1020	1020		1250	1150	10.13	300	- 50.	- 00 .
Absorbed Reboiler Duty [MW]	18.49	8.32	14.14	14.42	14.42	14.42	12.57	9.71	8.04	6.84	5.82	5.08	4.53
Heater Duty [MW]	20.54	9.24	15.71	16.02	16.02	16.02	13.97	10.78	8.94	7.60	6.47	5.65	5.03
Thermal Efficiency at 90%	90%	90%	90%	90%	90%	90%	90%	90%	90%	90%	90%	90%	90%
	1												
Fuel Gas HHV [MJ/kg]	49.494	49.494	49.494	49.494	49.494	49.494	49.494	49.494	49.494	49.494	49.494	49.494	49.494
Fuel Gas Requirement [kg/hr]	1494	672	1143	1165	1165	1165	1016	784	650	553	471	411	366
- 1 L Q/ J			1	1			1		1				
CO2 Emissions Factor [kg CO2 per kg FG]	2.626	2.626	2.626	2.626	2.626	2.626	2.626	2.626	2.626	2.626	2.626	2.626	2.626
CO2 Formed from Amine Unit FG [kg/hr]	3923	1765	3001	3060	3060	3060	2667	2059	1706	1451	1236	1079	961
CO2 Formed from Amine Unit FG [te per annum]	34,363	15,463	26,287	26,803	26,803	26,803	23,367	18,040	14,948	12,714	10,824	9,450	8,419

Appendix 4 - Teesside Schematics

Yet to be provided

10 Glossary

<u></u>	
ASEP	Aggregated System Entry Point (where more than one entry point exists)
Capex	Capital Expenditure
CATS	Central Area Transmission System (ie from the UK Continental Shelf)
CCGT	Combined Cycle Gas Turbine (a gas-fired electricity generation unit)
CV	Calorific Value
CH ₄	Methane
EU ETS	EU Emissions Trading System (multi-country, multi-sector greenhouse gas
	emissions trading system, see https://www.gov.uk/participating-in-the-eu-ets.)
FES	Future Energy Supply (document, available on nationalgrid.com)
GSMR	Gas Safety (Management) Regulations
GSOG	Gas Storage Operators Group
H ₂ S	Hydrogen Sulphide
ICF	Incomplete Combustion Factor
kte	Kilo tonnes equivalent (thousands of tonnes equivalent)
MERUK	Maximisation of Economic Recovery of oil and gas from the UK continental shelf
mol%	Mole % (a measure of the constituents in a mixture)
NEA	Network Entry Agreement
NPV10	Net Present Value discounted at 10%
OEM	Original Equipment Manufacturer
SI	Soot Index
te	Tonnes equivalent
TEG/MEG	Tri- and mono- ethylene glycols (commonly used in dewatering applications)
uHPHT	ultra-High Pressure High Temperature
WI	Wobbe Index (an indicator of the interchangeability of gas)